

## **L9 Part B**

# **Thermal characterization of homogeneous and heterogeneous materials using SVD techniques**

**Presented by**  
**Elena PALOMO DEL BARRIO**  
**I2M/TREFLE, Esplanade des Arts et Métier, 33405 Talence**  
**(Contact: [elena.palomo@trefle-u.bordeaux.fr](mailto:elena.palomo@trefle-u.bordeaux.fr))**

**PhD: A. Godin**  
**EXP: J.L. Dauvergne, C. Pradère**  
**NUM: E. Ahusborde, M. Azaiez**

$$\mathbf{Y} + \boldsymbol{\varepsilon} = \mathbf{M}\boldsymbol{\theta}$$

**Noise-corrupted  
observers**

**Sensitivity matrix**

Badly conditioned

Noise amplifier

**SVD of the observed  
thermal response**

**REGULARIZATION**

Experiment design

SVD of **M**

Cost function

etc.

# Materials & Objectives

## Homogeneous materials

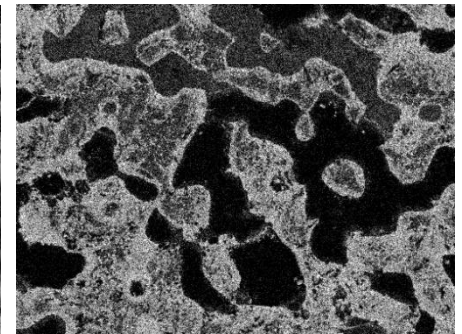
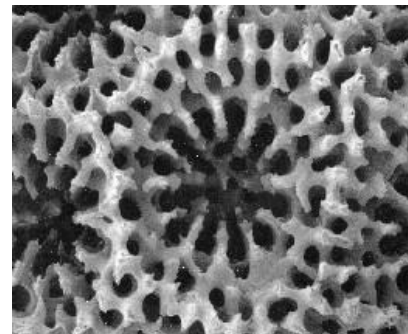
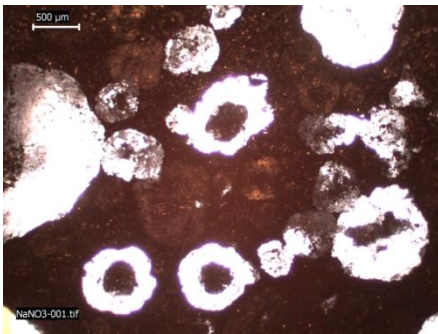
Diffusivity tensor

## Multi-phase materials

Phases discrimination & interfaces location

Diffusivity of the phases

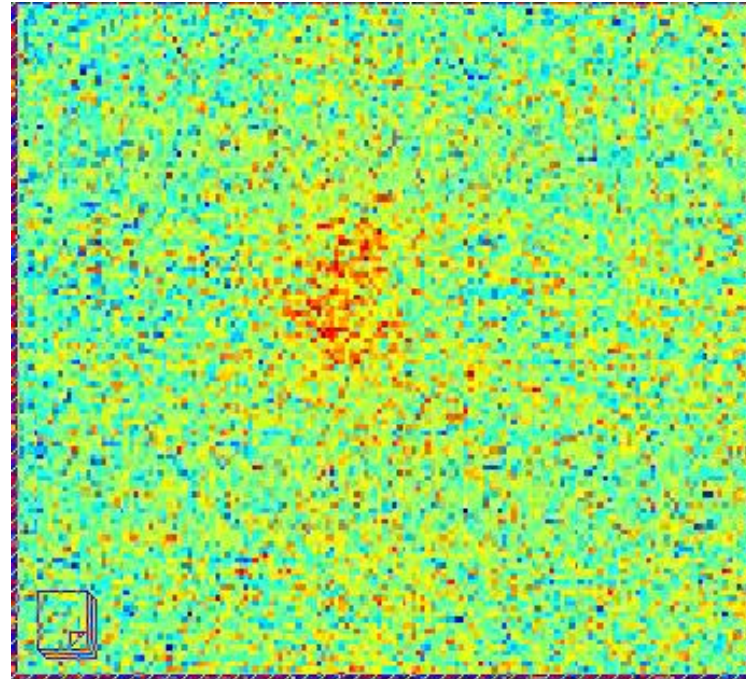
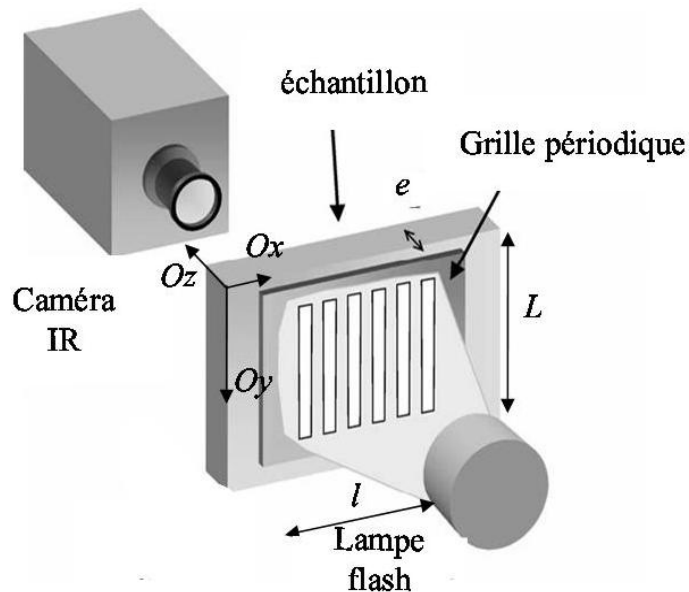
Thermal resistance at the interfaces



Scales:  $\mu\text{m}$  – cm

Thin samples - Infrared thermography

# Experimental framework

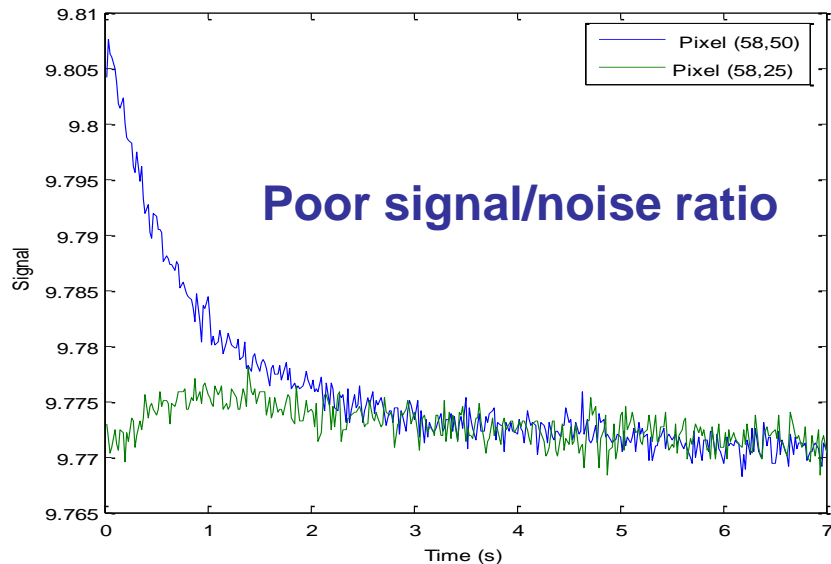
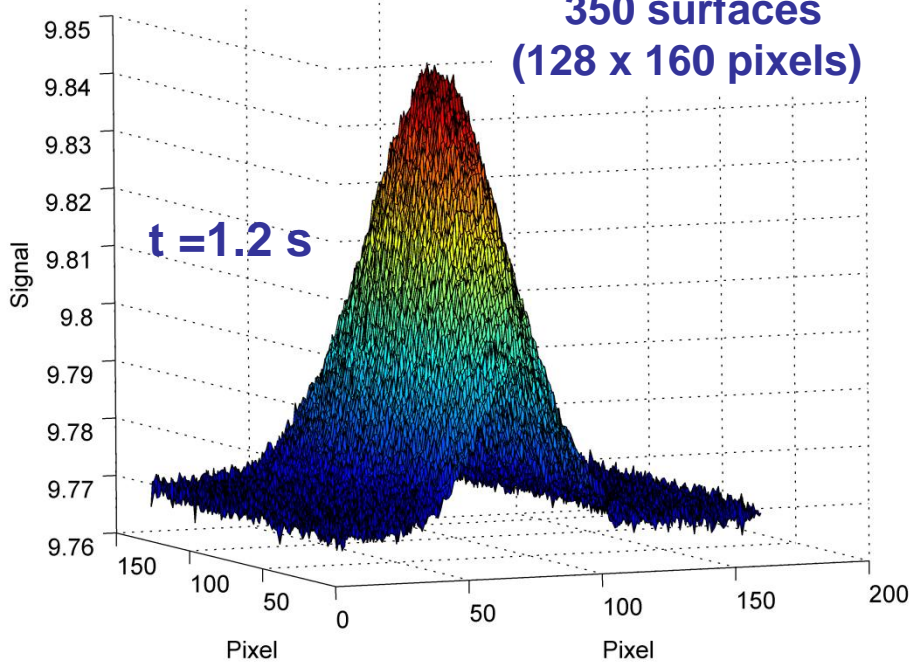


- Thin sample
- Photo-thermal excitation (i.e. laser, lamp):
  - Time: modulated, flash, step ...
  - Space: spot, motif, random ...
- Thermal response observation (rear or front face) by an IR camera equipped by a focal point array



**350 surfaces  
(128 x 160 pixels)**

**t = 1.2 s**



## HIGH DIMENSION

1 map = 250 x 250 pixels = 62 500 data  
1 exp. > 1000 maps  
Number of data > **60 millions of data !**

## POOR QUALITY DATA

Linearity -> Low amplitudes  
Noise -> Optics, resolution, env.

Analytical  
solutions  
Homogeneous  
materials  
Experimental  
conditions

## SVD-based methods

Dimension  
reduction  
Noise effects  
reduction  
Negligible bias

# SVD of the thermal field

**Proposed for the first time in 1901 by Pearson, re-invented many times during the XX century**

- Principal components analysis (PCA)
- Singular values decomposition (SVD)
- Karhunen-Loève decomposition (KLD)
- Proper orthogonal decomposition (POD)
- Hotteling transformation
- Empirical eigenfunctions
- ....

## **Application fields**

- Data analysis (graphics, statistics ...)
- Forms recognition, faults detection ...
- Models reduction (turbulence)
- ...

**A tool providing optimal low-dimensional approximations of high-dimensional (infinite-dimensional) problems**

$$T(\mathbf{x}, t)$$

## **THERMAL FIELD**

space-time dependent function in a bounded region verifying

$$\forall t, \quad \int_{\Omega} T^2(\mathbf{x}, t) dx < \infty$$

## THERMAL FIELD - SVD

Projection on the orthogonal basis defined by the spectral decomposition of the ENERGY FUNCTION

$$W(\mathbf{x}, \mathbf{x}') \equiv \int_t T(\mathbf{x}, t) T(\mathbf{x}', t) dt = \sum_{m=1}^{\infty} \sigma_m^2 V_m(\mathbf{x}) V_m(\mathbf{x}')$$

$$\sigma_1^2 \geq \sigma_2^2 \geq \dots \geq 0$$

$$\text{Total energy} \quad \int_{\Omega} W(\mathbf{x}, \mathbf{x}) d\mathbf{x} = \sum_{m=1}^{\infty} \sigma_m^2$$

$$\forall t, T(\mathbf{x}, t) = \sum_{m=1}^{\infty} V_m(\mathbf{x}) z_m(t)$$

Orthogonal eigenfunctions

$$\langle V_k, V_m \rangle_{\Omega} \equiv \int_{\Omega} V_k(\mathbf{x}) V_m(\mathbf{x}) d\mathbf{x} = \delta_{km}$$

Orthogonal states

$$\langle z_m(t), z_k(t) \rangle_t \equiv \int_t z_m(t) z_k(t) dt = \delta_{mk} \sigma_m^2$$

## Optimal/closest linear $r$ -dimensional approximations

Best approximation in the sens of unitarily invariant norms

$$\forall t, T_r(\mathbf{x}, t) = \sum_{m=1}^r V_m(\mathbf{x}) z_m(t)$$

$$\|e_r\|^2 \equiv \int_t \int_{\Omega} e_r(\mathbf{x}, t) d\mathbf{x} dt = \sum_{m=r+1}^{\infty} \sigma_m^2$$

$$\forall t, e_r(\mathbf{x}, t) \equiv T(\mathbf{x}, t) - T_r(\mathbf{x}, t)$$

## An excellent tool for data reduction

High quality approximations of the thermal field can often be reached with a very low number of eigenelements

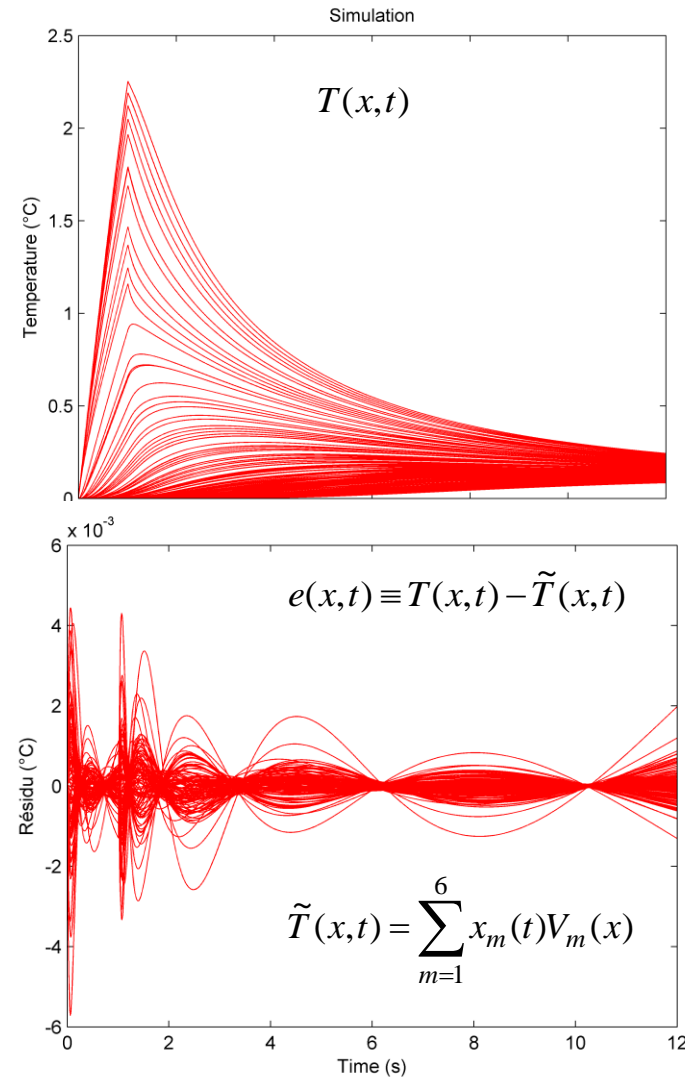
### EXAMPLE

1 map =  $250 \times 250 = 62500$  pixels  
1000 sampling times

1000 maps x 62500 pixels/map =  
= 62.5 millions data

> 99% reduction

6 maps of 62500 pixels  
+ 6 time series of length 1000  
= 380 000 data



Thermal response of a thin plate (6mm x 6mm) excited by a laser spot during 1s


## Noise propagation through SVD

$$\tilde{T}(\mathbf{x}, t) = T(\mathbf{x}, t) + \varepsilon(\mathbf{x}, t)$$

$$\forall \mathbf{x}, \mathbf{x}' \quad W_{\varepsilon}(\mathbf{x}, \mathbf{x}') \equiv \int_t \varepsilon(\mathbf{x}, t) \varepsilon(\mathbf{x}', t) dt = \sigma_{\varepsilon}^2 \delta(\mathbf{x} - \mathbf{x}')$$

**(1)** spatially-uncorrelated noise has no effect on eigenfunctions, the noise being entirely reported on states

$$\tilde{W}(\mathbf{x}, \mathbf{x}') = W(\mathbf{x}, \mathbf{x}') + W_{\varepsilon}(\mathbf{x}, \mathbf{x}') = \sum_{m=1}^{\infty} V_m(\mathbf{x}) \tilde{\sigma}_m^2 V_m(\mathbf{x}') \quad \text{with} \quad \tilde{\sigma}_m^2 = \sigma_m^2 + \sigma_{\varepsilon}^2 \delta(\mathbf{x} - \mathbf{x}')$$



$$\tilde{T}(\mathbf{x}, t) = \sum_{m=1}^{\infty} V_m(\mathbf{x}) \tilde{z}_m(t)$$

$$\tilde{z}_m(t) = \int_{\Omega} \tilde{T}(\mathbf{x}, t) V_m(\mathbf{x}) d\mathbf{x} = \int_{\Omega} T(\mathbf{x}, t) V_m(\mathbf{x}) dx + \int_{\Omega} \varepsilon(\mathbf{x}, t) V_m(\mathbf{x}) dx = z_m(t) + \underline{\gamma_m(t)}$$

$$\forall m, \quad \sigma_{\varepsilon, m}^2 \equiv \int_t \gamma_m^2(t) dt = \sigma_{\varepsilon}^2$$

$$\text{noise} / \text{signal} = \sigma_{\varepsilon}^2 / \sigma_m^2$$

$$I(\mathbf{x}) \equiv \frac{\int_t T^2(\mathbf{x}, t) dt}{\int_t \varepsilon^2(\mathbf{x}, t) dt} = \frac{\sum_{m=1}^{\infty} V_m^2(\mathbf{x}) \sigma_m^2}{\sum_{m=1}^{\infty} V_m^2(\mathbf{x}) \sigma_{\varepsilon}^2}$$

$$I_r(\mathbf{x}) = \frac{\sum_{m=1}^r V_m^2(\mathbf{x}) \sigma_m^2}{\sum_{m=1}^r V_m^2(\mathbf{x}) \sigma_{\varepsilon}^2}$$

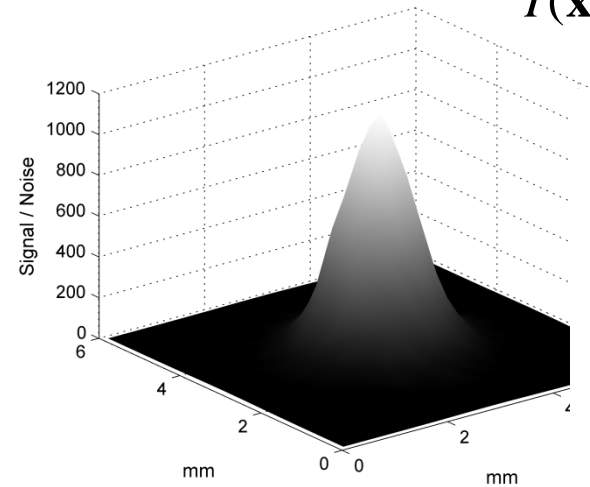
**(2)** SVD truncation acts as a signal/noise ratio amplifier

$$\frac{I(\mathbf{x})}{I_r(\mathbf{x})} = \underbrace{\left( 1 + \frac{\sum_{m=r+1}^{\infty} V_m^2(\mathbf{x}) \sigma_m^2}{\sum_{m=1}^r V_m^2(\mathbf{x}) \sigma_m^2} \right)}_{O(1)} \left( \frac{\sum_{m=1}^r V_m^2(\mathbf{x})}{\sum_{m=1}^{\infty} V_m^2(\mathbf{x})} \right) \approx \left( \frac{\sum_{m=1}^r V_m^2(\mathbf{x})}{\sum_{m=1}^{\infty} V_m^2(\mathbf{x})} \right) < 1$$

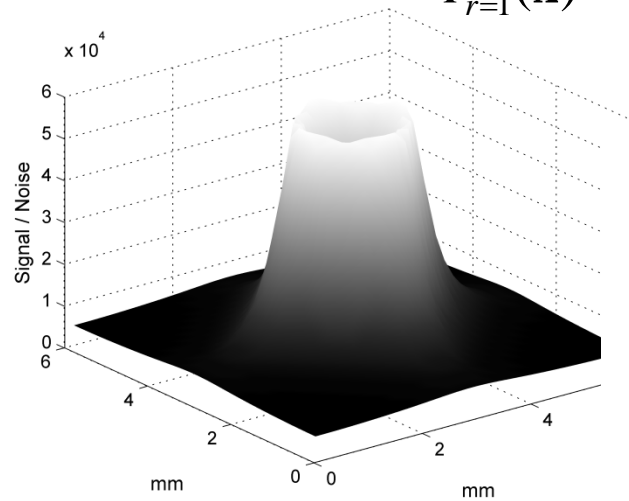
$$\sigma_1^2 \gg \sigma_2^2 \gg \dots \geq 0$$

Signal/noise amplification is as much significant as the dimension of the approximation reduces

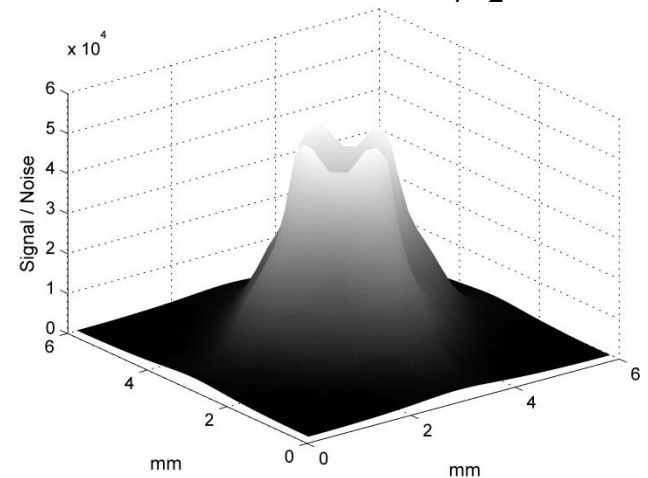
$I(\mathbf{x})$



$I_{r=1}(\mathbf{x})$

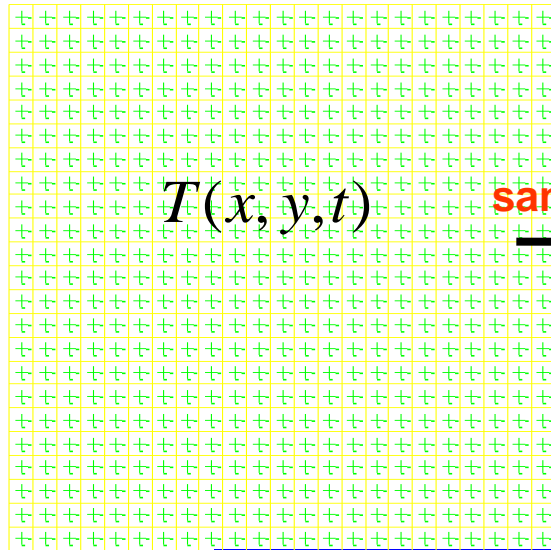


$I_{r=2}(\mathbf{x})$

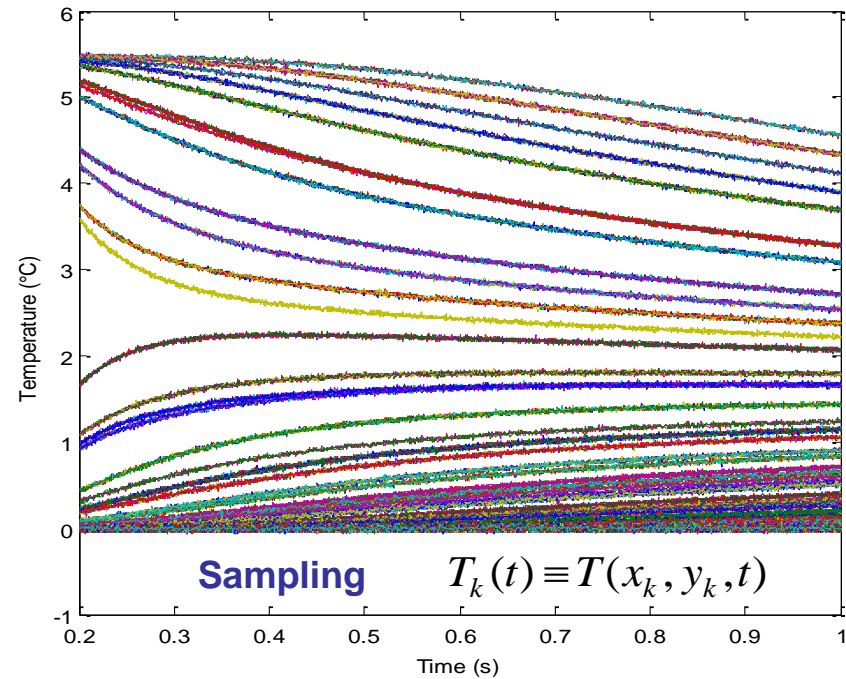




# SVD in practice



sampling



Time-dependent  
vector of high  
dimension (n x 1)

$$\mathbf{T}(t) = \begin{bmatrix} T_1(t) \\ T_2(t) \\ \vdots \\ T_n(t) \end{bmatrix}$$

Energy matrix (n x n)  
& Spectral decomposition

$$\mathbf{W} = \int_{t=t_o}^{t_f} \mathbf{T}(t) \mathbf{T}^t(t) dt$$

$$\mathbf{W} = \mathbf{V} \mathbf{\Sigma} \mathbf{V}^t$$

Matrix of eigenfunctions  
 $\mathbf{V}_m(x, y)$  column-wise  
placed

Diagonal matrix of eigen-  
values  $\sigma_1^2 > \sigma_2^2 > \dots > 0$

Vector of states

$$\mathbf{Z}(t) \equiv \begin{bmatrix} z_1(t) \\ z_2(t) \\ \vdots \\ z_n(t) \end{bmatrix} = \mathbf{V}^t \mathbf{T}(t)$$

# Homogeneous materials

$$\Omega: 0 < x < L_x, 0 < y < L_y$$

Photo thermal perturbation – Establishment of a initial temperature field for further estimations

Photo-thermal excitation (i.e. laser, lamp)

Time: modulated, flash, step ...

Space: spot, motif, random ...

$$\frac{\partial T(x, y, t)}{\partial t} = \alpha_x \frac{\partial^2 T(x, y, t)}{\partial x^2} + \alpha_y \frac{\partial^2 T(x, y, t)}{\partial y^2} - \beta T(x, y, t) + \varphi(x, y, t)$$

$$\left. \frac{\partial T(x, y, t)}{\partial x} \right|_{x=0, L_x} = 0, \quad \left. \frac{\partial T(x, y, t)}{\partial y} \right|_{y=0, L_y} = 0 \quad T(x, y, 0) = 0$$

Equations governing thermal relaxation of the initial temperature field

$$\frac{\partial T(x, y, t)}{\partial t} = \alpha_x \frac{\partial^2 T(x, y, t)}{\partial x^2} + \alpha_y \frac{\partial^2 T(x, y, t)}{\partial y^2} - \beta T(x, y, t)$$

$$\left. \frac{\partial T(x, y, t)}{\partial x} \right|_{x=0, L_x} = 0, \quad \left. \frac{\partial T(x, y, t)}{\partial y} \right|_{y=0, L_y} = 0 \quad T(x, y, 0) = T_o(x, y)$$

**ESTIMATION**

$\alpha_x, \alpha_y, \beta$

$$\frac{\partial T(x, y, t)}{\partial t} = \alpha_x \frac{\partial^2 T(x, y, t)}{\partial x^2} + \alpha_y \frac{\partial^2 T(x, y, t)}{\partial y^2} - \beta T(x, y, t)$$

+ adiabatic boundary conditions

$$T(x, y, t) = \sum_{m=1}^{\infty} V_m(x, y) z_m(t)$$

$$\langle V_k, V_m \rangle_{\Omega} \equiv \int_{\Omega} V_k(x) V_m(x) dx = \delta_{km}$$

$$\langle z_m(t), z_k(t) \rangle_t \equiv \int_t z_m(t) z_k(t) dt = \delta_{mk} \sigma_m^2$$

$$\frac{1}{\sigma_k^2} \left\langle \frac{dz_i(t)}{dt}, z_k(t) \right\rangle_t = \frac{1}{\sigma_i^2} \left\langle \frac{dz_k(t)}{dt}, z_i(t) \right\rangle_t$$

Integration  
over  $\Omega$

$$\frac{d \langle T(x, y, t) \rangle_{\Omega}}{dt} = -\beta \langle T(x, y, t) \rangle_{\Omega}$$

**ESTIMATION  $\beta$**   
linear least squares  
methods

$$\left\langle \langle \circ, V_k \rangle_{\Omega}, z_i(t) \right\rangle_t$$

$$i = 1, 2, 3, \dots; \quad k = i, i+1, i+2, \dots$$

$$y_{ik} = \alpha_x \left\langle \frac{\partial^2 V_i(x, y)}{\partial x^2}, V_k(x, y) \right\rangle_{\Omega} + \alpha_y \left\langle \frac{\partial^2 V_i(x, y)}{\partial y^2}, V_k(x, y) \right\rangle_{\Omega}$$

$$y_{ik} = \frac{z_i(t_f) z_k(t_f) - z_i(0) z_k(0)}{\sigma_i^2 + \sigma_k^2} + \beta \delta_{ik}$$

$$y_{ik} = \frac{z_i(t_f)z_k(t_f) - z_i(0)z_k(0)}{\sigma_i^2 + \sigma_k^2} + \beta\delta_{ik}$$

$$\tilde{z}_{i,k}(t_f) = z_{i,k}(t_f) + \varepsilon_{i,k}(t_f)$$

$$\tilde{z}_{i,k}(0) = z_{i,k}(0) + \varepsilon_{i,k}(0)$$

$$\tilde{\sigma}_i^2 = \sigma_i^2 + \sigma_\varepsilon^2$$

$$\tilde{\beta} = \beta + \varepsilon_\beta$$

How many equations, which ones ?

$$\tilde{y}_{ik} = y_{ik} \frac{1}{1 + 2\left(\frac{\sigma_\varepsilon^2}{\sigma_i^2 + \sigma_k^2}\right)} + \frac{f(\text{noise}_z)}{\sigma_i^2 + \sigma_k^2 + 2\sigma_\varepsilon^2} + \varepsilon_\beta \delta_{ik}$$

$$E[\tilde{y}_{ik}] = y_{ik} \frac{1}{1 + 2\left(\frac{\sigma_\varepsilon^2}{\sigma_i^2 + \sigma_k^2}\right)} \quad \text{bias}$$

$$\begin{aligned} \text{var}_y &\equiv E[(\tilde{y}_{ik} - y_{ik})^2] = \\ &= \frac{z_k^2(t_f) + z_i^2(t_f) + z_k^2(0) + z_i^2(0)}{(\sigma_i^2 + \sigma_k^2 + 2\sigma_\varepsilon^2)^2} \text{var}_\varepsilon + \text{var}_\beta \delta_{ik} \end{aligned}$$

$$\sigma_1^2 \geq \sigma_2^2 \geq \dots \geq 0 \quad \sigma_1^2 \gg \sigma_2^2 \gg \dots \geq 0$$

$$\sigma_\varepsilon^2 \ll \sigma_i^2 + \sigma_k^2$$

Ordering by  
decreasing

$$\sigma_i^2 + \sigma_k^2$$

Cut-off

$$y_{11}$$

$$y_{12}$$

$$y_{22}$$

$$\vdots$$

Adding a  
more one =  
Increasing  
bias

## Two unknown parameters – Two equations for estimations

$$y_{11} = \alpha_x \left\langle \frac{\partial^2 V_1(x, y)}{\partial x^2}, V_1(x, y) \right\rangle_{\Omega} + \alpha_y \left\langle \frac{\partial^2 V_1(x, y)}{\partial y^2}, V_1(x, y) \right\rangle_{\Omega}$$

$$y_{12} = \alpha_x \left\langle \frac{\partial^2 V_1(x, y)}{\partial x^2}, V_2(x, y) \right\rangle_{\Omega} + \alpha_y \left\langle \frac{\partial^2 V_1(x, y)}{\partial y^2}, V_2(x, y) \right\rangle_{\Omega}$$

**$(\alpha_x, \alpha_y)$  ESTIMATE**

$$\begin{bmatrix} \hat{\alpha}_x \\ \hat{\alpha}_y \end{bmatrix} = \mathbf{M}^{-1} \mathbf{y}$$

with:

$$\mathbf{y} = \begin{bmatrix} \Delta \tilde{z}_1 \tilde{z}_1 / (\tilde{\sigma}_1^2 + \tilde{\sigma}_1^2) + \hat{\beta} \\ \Delta \tilde{z}_1 \tilde{z}_2 / (\tilde{\sigma}_1^2 + \tilde{\sigma}_2^2) \end{bmatrix}$$

$$\mathbf{M} = \begin{bmatrix} \left\langle \frac{\partial^2 V_1(x, y)}{\partial x^2}, V_1(x, y) \right\rangle_{\Omega} & \left\langle \frac{\partial^2 V_1(x, y)}{\partial y^2}, V_1(x, y) \right\rangle_{\Omega} \\ \left\langle \frac{\partial^2 V_1(x, y)}{\partial x^2}, V_2(x, y) \right\rangle_{\Omega} & \left\langle \frac{\partial^2 V_1(x, y)}{\partial y^2}, V_2(x, y) \right\rangle_{\Omega} \end{bmatrix}$$

$$\mathbb{E}[\hat{\alpha}_x] = \alpha_x; \quad \mathbb{E}[\hat{\alpha}_y] = \alpha_y$$

provided that:  $\sigma_{\varepsilon}^2 \ll \sigma_1^2 + \sigma_2^2$

# NUMERICAL EXAMPLES

Noise amplitude: 0.02, 0.1°C, 0.5°C, 1°C

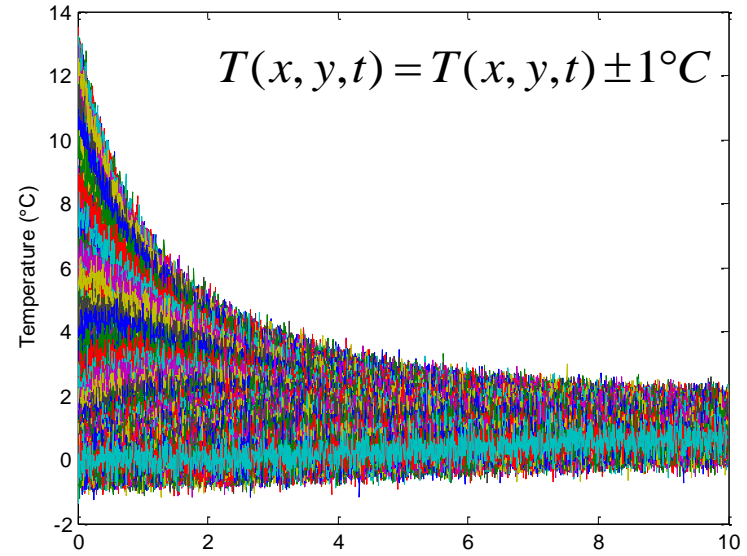
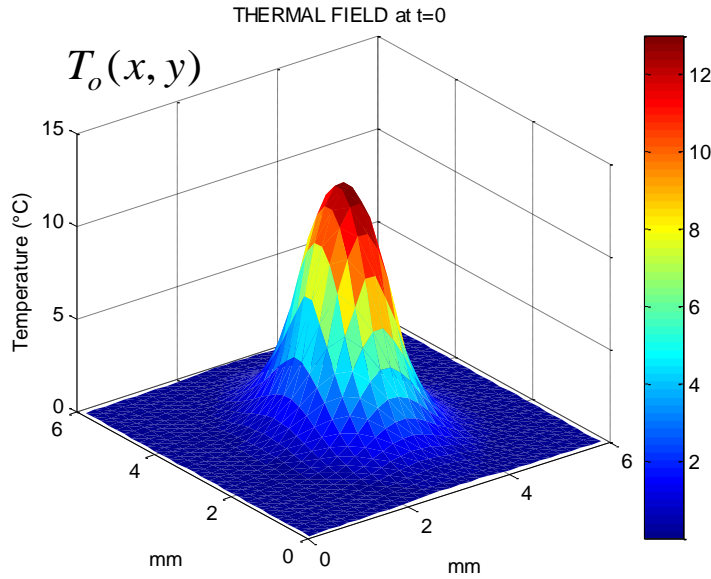


Table 3. Estimated values for thermal parameters. True values are

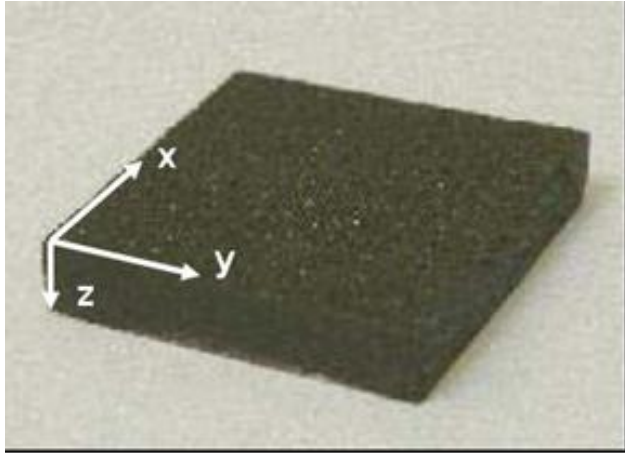
$\beta = 0.152 s^{-1}$ ,  $\alpha_x = 0.1515 \times 10^{-6} m^2.s^{-1}$  and  $\alpha_y = 0.3030 \times 10^{-6} m^2.s^{-1}$ .

Noise ampl. (°C)	$\hat{\beta}$ ( $s^{-1}$ )	$\left  \frac{\beta - \hat{\beta}}{\beta} \right  \times 100$	$\hat{\alpha}_x$ ( $\times 10^{-6} m^2.s^{-1}$ )	$\left  \frac{\alpha_x - \hat{\alpha}_x}{\alpha_x} \right  \times 100$	$\hat{\alpha}_y$ ( $\times 10^{-6} m^2.s^{-1}$ )	$\left  \frac{\alpha_y - \hat{\alpha}_y}{\alpha_y} \right  \times 100$
$\pm 1.00$	0.0152 ( $\pm 0.5 \times 10^{-3}$ )	0.055	0.1572 ( $\pm 0.02$ )	3.72	0.2889 ( $\pm 0.036$ )	4.66
$\pm 0.50$	0.0152 ( $\pm 0.2 \times 10^{-3}$ )	0.06	0.1540 ( $\pm 0.007$ )	1.62	0.2989 ( $\pm 0.0162$ )	1.37
$\pm 0.10$	0.0152 ( $\pm 0.04 \times 10^{-3}$ )	0.002	0.1517 ( $\pm 0.0015$ )	0.12	0.3026 ( $\pm 0.0037$ )	0.15
$\pm 0.02$	0.0152 ( $\pm 0.01 \times 10^{-3}$ )	0.0007	0.1515 ( $\pm 0.0003$ )	0.022	0.3029 ( $\pm 0.0007$ )	0.0003

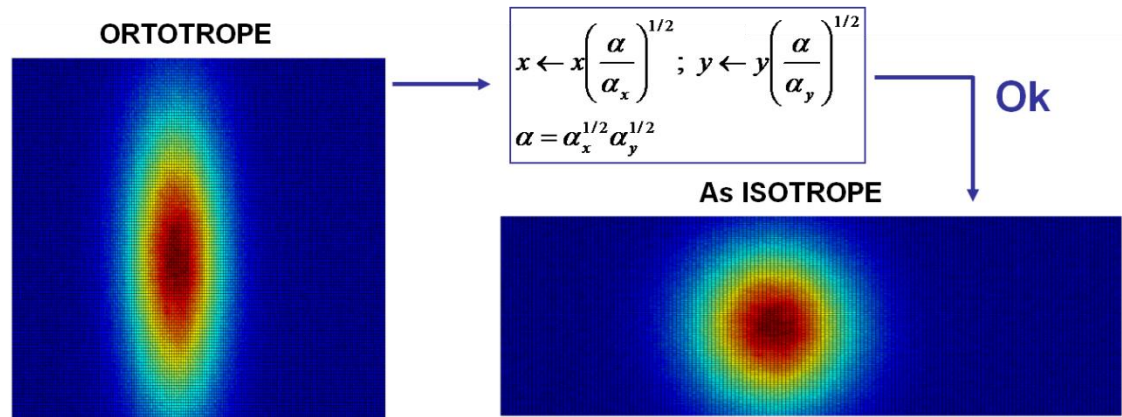
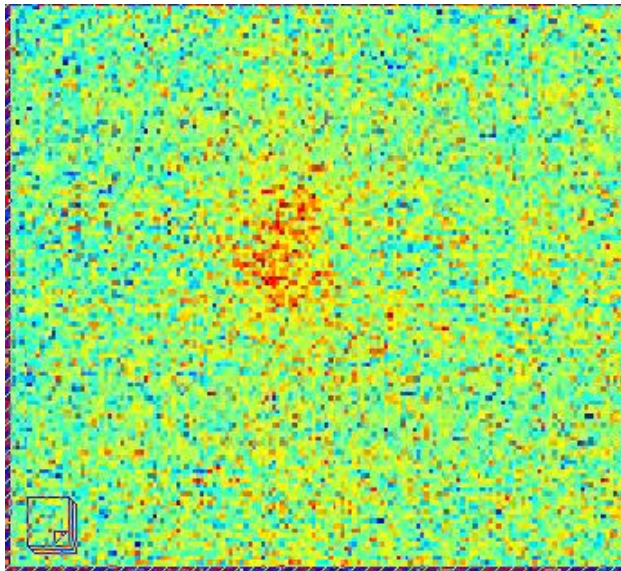


# EXPERIMENTAL TEST

## Carbon/Epoxy composite material



	ICAM CETHIL	TREFLE
$\alpha_x$ (m <sup>2</sup> /s)	$4 \times 10^{-7}$	$3.80 \times 10^{-7}$
$\alpha_y$ (m <sup>2</sup> /s)	$3.5 \times 10^{-6}$	$3.54 \times 10^{-6}$

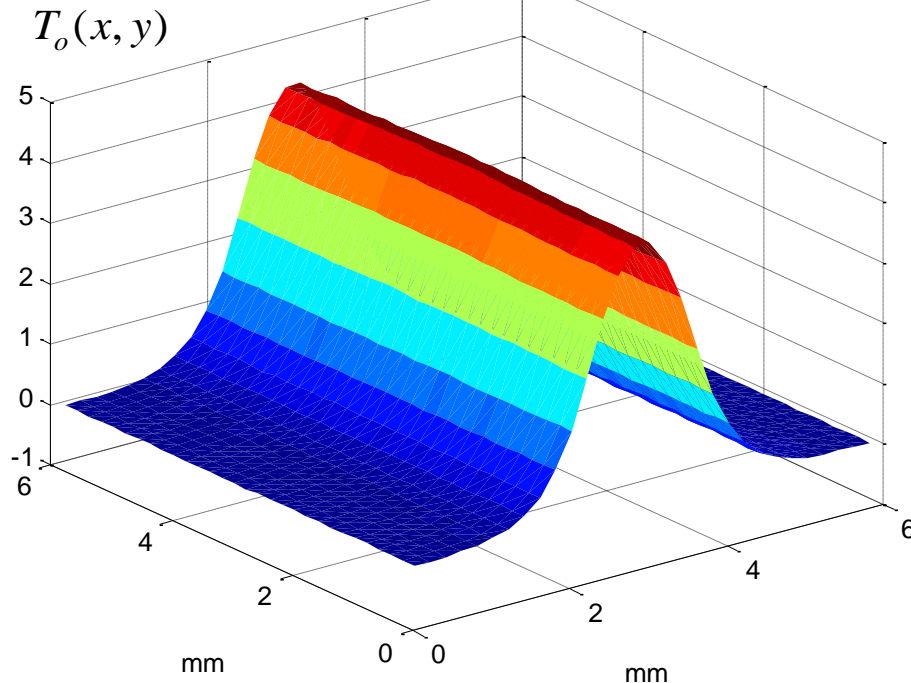


$$\beta = 0.152 s^{-1} \quad \alpha_x = 1.515 \times 10^{-7} m^2.s^{-1} \quad \alpha_y = 3.030 \times 10^{-7} m^2.s^{-1}$$

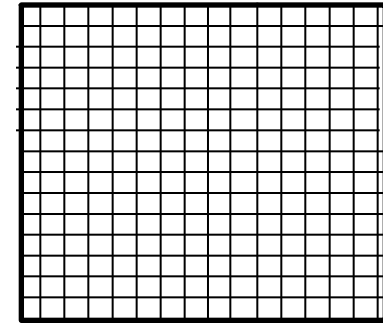
## Many other numerical tests for reliability analysis

Much more high beta (x100)  
 Much more high diffusivities (x1000)  
 Much more low diffusivities (/1000)  
 Much more high  $\alpha_x/\alpha_y$  ( $\sim 100$ ,  $\sim 1000$ )  
 Much more low  $\alpha_x/\alpha_y$

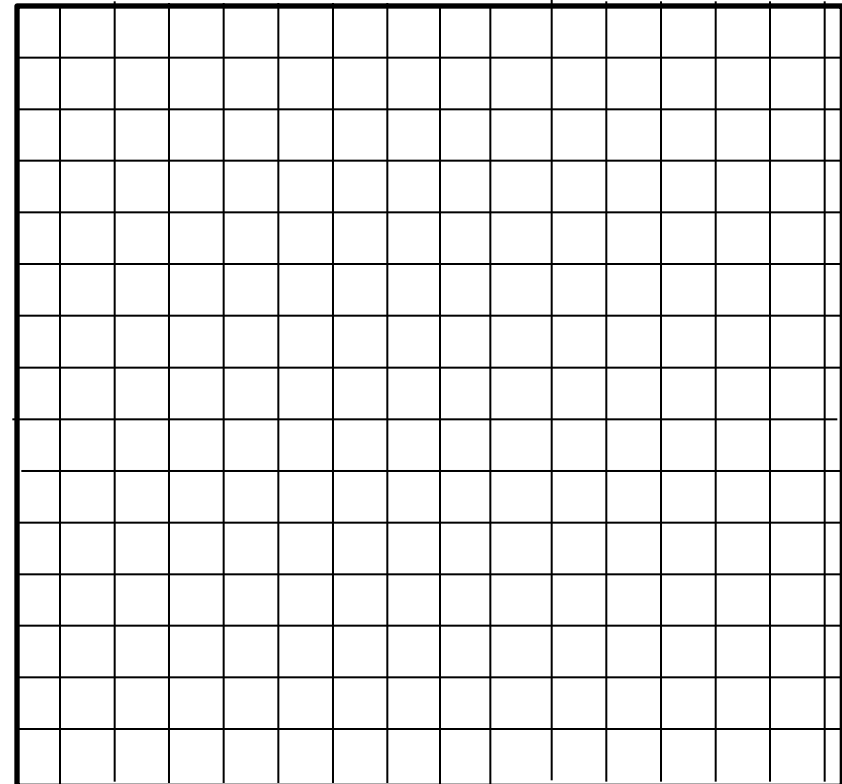
$$\alpha_x / \alpha_y = 1000$$



Higher resolution - Smaller area



Greater area – Lower resolution



## Many other numerical tests for reliability analysis

- Much more high beta (x100)
- Much more high diffusivities (x1000)
- Much more low diffusivities (/1000)
- Much more high  $\alpha_x/\alpha_y$  (~100, ~1000)
- Much more low  $\alpha_x/\alpha_y$  (i.e.  $\alpha_x/\alpha_y = 1.01$ )

Table 3. Estimated values for thermal parameters. True values are  $\beta = 0.152 s^{-1}$ ,  $\alpha_x = 0.1515 \times 10^{-6} m^2.s^{-1}$  and  $\alpha_y = 0.3030 \times 10^{-6} m^2.s^{-1}$ .

Noise ampl. (°C)	$\hat{\beta}$ ( $s^{-1}$ )	$\left  \frac{\beta - \hat{\beta}}{\beta} \right  \times 100$	$\hat{\alpha}_x$ ( $\times 10^{-6} m^2 s^{-1}$ )	$\left  \frac{\alpha_x - \hat{\alpha}_x}{\alpha_x} \right  \times 100$	$\hat{\alpha}_y$ ( $\times 10^{-6} m^2 s^{-1}$ )	$\left  \frac{\alpha_y - \hat{\alpha}_y}{\alpha_y} \right  \times 100$
$\pm 1.00$	0.0152 ( $\pm 0.5 \times 10^{-3}$ )	0.055	0.1572 ( $\pm 0.02$ )	3.72	0.2889 ( $\pm 0.036$ )	4.66
$\pm 0.50$	0.0152 ( $\pm 0.2 \times 10^{-3}$ )	0.06	0.1540 ( $\pm 0.007$ )	1.62	0.2989 ( $\pm 0.0162$ )	1.37
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**Estimation improvement required**

# ESTIMATIONS IMPROVEMENT

## Cumulative integral-SVD method

$$\frac{\partial T(x, y, t)}{\partial t} = \alpha_x \frac{\partial^2 T(x, y, t)}{\partial x^2} + \alpha_y \frac{\partial^2 T(x, y, t)}{\partial y^2} - \beta T(x, y, t)$$

+ adiabatic boundary conditions

$$\Delta T(x, y, t) = \alpha_x \frac{\partial^2 u(x, y, t)}{\partial x^2} + \alpha_y \frac{\partial^2 u(x, y, t)}{\partial y^2} - \beta u(x, y, t)$$

+ adiabatic boundary conditions &  $\Delta T(x, y, t) = T(x, y, t) - T_o(x, y)$

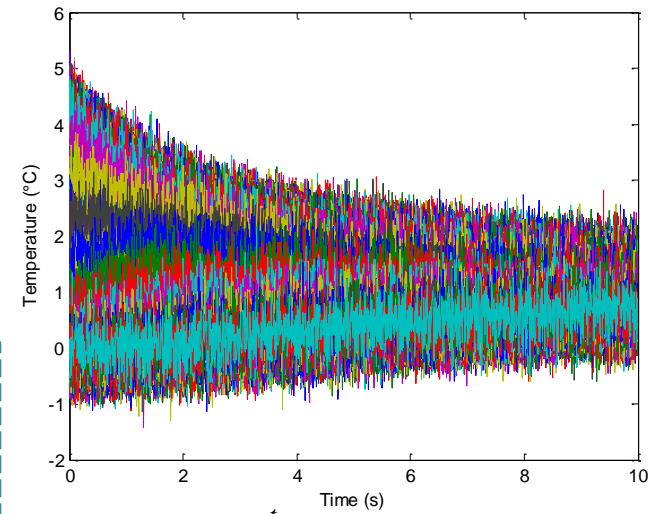
**SVD:**  $u(x, y, t) = \sum_{m=1}^{\infty} V_m(x, y) z_m(t)$

Projection:  $\Delta T(x, y, t) = \sum_{m=1}^{\infty} V_m(x, y) \eta_m(t)$

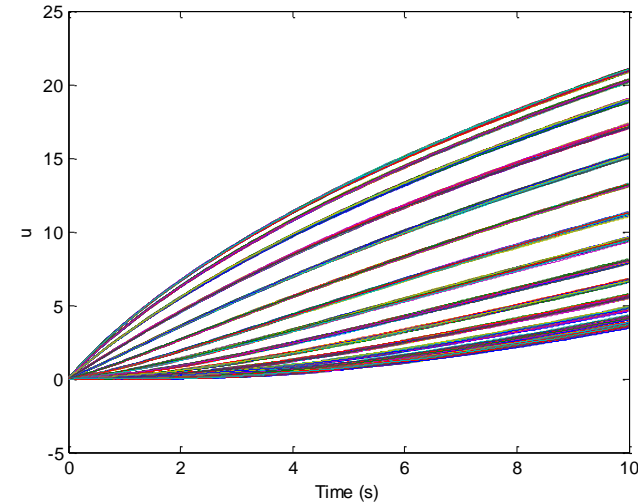
$$\begin{bmatrix} \hat{\alpha}_x \\ \hat{\alpha}_y \end{bmatrix} = \mathbf{M}^{-1} \mathbf{y}$$

$$\mathbf{y} = \begin{bmatrix} \langle \tilde{z}_1 \tilde{\eta}_1 \rangle_t / \tilde{\sigma}_1^2 + \hat{\beta} \\ \langle \tilde{z}_1 \tilde{\eta}_2 \rangle_t / \tilde{\sigma}_1^2 \end{bmatrix}$$

$$\mathbf{M} = \begin{bmatrix} \langle \partial_x^2 V_1(x, y), V_1(x, y) \rangle_{\Omega} & \langle \partial_y^2 V_1(x, y), V_1(x, y) \rangle_{\Omega} \\ \langle \partial_x^2 V_1(x, y), V_2(x, y) \rangle_{\Omega} & \langle \partial_y^2 V_1(x, y), V_2(x, y) \rangle_{\Omega} \end{bmatrix}$$



$$u(x, y, t) = \int_0^t T(x, y, \tau) d\tau$$



# ESTIMATIONS IMPROVEMENT

## Modal-SVD method

$$\frac{\partial T(x, y, t)}{\partial t} = \alpha_x \frac{\partial^2 T(x, y, t)}{\partial x^2} + \alpha_y \frac{\partial^2 T(x, y, t)}{\partial y^2} - \beta T(x, y, t)$$

+ adiabatic boundary conditions

$$\left\{ \begin{array}{l} T(x, y, t) = \sum_{m=1}^{\infty} V_m(x, y) z_m(t) \\ \langle \circ, z_j(t) \rangle_t \\ \langle z_m(t), z_j(t) \rangle_t \equiv \int_t z_m(t) z_j(t) dt = \delta_{mj} \sigma_j^2 \end{array} \right.$$

Set of coupled PDE  
for eigenfunctions

$$\alpha_x \frac{\partial^2 V_j(x, y)}{\partial x^2} + \alpha_y \frac{\partial^2 V_j(x, y)}{\partial y^2} - \beta V_j(x, y) = \sum_{m=1}^{\infty} V_m(x, y) a_{mj}$$

+ adiabatic boundary conditions

$$\text{with: } \forall(m, j) \quad a_{mj} = a_{jm} = \frac{z_m(t_f) z_j(t_f) - z_m(0) z_j(0)}{\sigma_m^2 + \sigma_j^2}$$

$$\alpha_x \begin{bmatrix} \partial_x^2 V_1(x, y) \\ \partial_x^2 V_2(x, y) \\ \vdots \end{bmatrix} + \alpha_y \begin{bmatrix} \partial_y^2 V_1(x, y) \\ \partial_y^2 V_2(x, y) \\ \vdots \end{bmatrix} - \beta \begin{bmatrix} V_1(x, y) \\ V_2(x, y) \\ \vdots \end{bmatrix} = \mathbf{A} \begin{bmatrix} V_1(x, y) \\ V_2(x, y) \\ \vdots \end{bmatrix}$$

$$\begin{bmatrix} \phi_1(x, y) \\ \phi_2(x, y) \\ \vdots \end{bmatrix} = \mathbf{P}^t \begin{bmatrix} V_1(x, y) \\ V_2(x, y) \\ \vdots \end{bmatrix}$$

$$\mathbf{A} = \mathbf{P} \mathbf{\Sigma} \mathbf{P}^t$$

$$\mathbf{P}^t \mathbf{P} = \mathbf{I}; \quad \mathbf{\Sigma} = \text{diag}\{\lambda_j\}$$

$$\mathbf{A} = \{a_{mi}\}$$

$$a_{mi} = \frac{z_m(t_f)z_i(t_f) - z_m(0)z_i(0)}{\sigma_m^2 + \sigma_i^2}$$

Set of independent PDE

$$\alpha_x \frac{\partial^2 \phi_j(x, y)}{\partial x^2} + \alpha_y \frac{\partial^2 \phi_j(x, y)}{\partial y^2} - \beta \phi_j(x, y) = \lambda_j \phi_j(x, y)$$

+ adiabatic boundary conditions

Eigenfunctions/Eigenvalues  
problem associated to the  
thermal equations



## Set of independent PDE

$$\alpha_x \frac{\partial^2 \phi_j(x, y)}{\partial x^2} + \alpha_y \frac{\partial^2 \phi_j(x, y)}{\partial y^2} - \beta \phi_j(x, y) = \lambda_j \phi_j(x, y)$$

+ adiabatic boundary conditions

Eigenfunctions/Eigenvalues problem associated to the thermal equations

Orthomormal  $\longrightarrow$   $\left\{ \begin{array}{l} \alpha_x \langle \partial_x^2 \phi_j(x, y), \phi_j(x, y) \rangle_{\Omega} + \alpha_y \langle \partial_y^2 \phi_j(x, y), \phi_j(x, y) \rangle = \lambda_j + \beta \\ \alpha_x \langle \partial_x^2 \phi_j(x, y), \phi_k(x, y) \rangle_{\Omega} + \alpha_y \langle \partial_y^2 \phi_j(x, y), \phi_k(x, y) \rangle = 0 \end{array} \right.$

$\phi_j(x, y)$

Analytical  $\longrightarrow$   $\left\{ \begin{array}{l} \phi_j(x, y) = (2/L) \cos(\kappa_p x) \cos(\gamma_s y) \\ \kappa_p = p\pi/L; \gamma_s = s\pi/L; \langle \partial_x^2 \phi_j, \phi_j \rangle = -\kappa_p^2; \langle \partial_y^2 \phi_j, \phi_j \rangle = -\gamma_s^2 \end{array} \right.$



$$\alpha_x \kappa_{pj}^2 + \alpha_y \gamma_{sj}^2 = -(\lambda_j + \beta)$$

## IN PRACTICE - Without noise

$$\alpha_x \frac{\partial^2 V_j(x, y)}{\partial x^2} + \alpha_y \frac{\partial^2 V_j(x, y)}{\partial y^2} - \beta V_j(x, y) = \sum_{m=1}^{\infty} V_m(x, y) a_{mj}$$

$$[\alpha_x \mathbf{L}_x + \alpha_y \mathbf{L}_y - \beta \mathbf{I}] \mathbf{V} = \mathbf{V} \mathbf{A}$$

$$\mathbf{A} = \mathbf{P} \mathbf{\Sigma} \mathbf{P}^t$$

$$\boldsymbol{\varphi} = \mathbf{V} \mathbf{P}$$

$$\underbrace{\alpha_x \boldsymbol{\varphi}^t \mathbf{L}_x \boldsymbol{\varphi}}_{\text{diag}} + \underbrace{\alpha_y \boldsymbol{\varphi}^t \mathbf{L}_y \boldsymbol{\varphi}}_{\text{diag}} = \mathbf{\Sigma} + \beta \mathbf{I}$$

$n$  equations

$$\alpha_x \kappa_{pj}^2 + \alpha_y \gamma_{sj}^2 = -(\lambda_j + \beta)$$

$$[\alpha_x \mathbf{L}_x + \alpha_y \mathbf{L}_y - \beta \mathbf{I}] [\mathbf{V}_d \quad \mathbf{V}_f] = [\mathbf{V}_d \quad \mathbf{V}_f] \begin{bmatrix} \mathbf{A}_{dd} & \mathbf{A}_{fd} \\ \mathbf{A}_{fd} & \mathbf{A}_{ff} \end{bmatrix}$$

$$[\alpha_x \mathbf{L}_x + \alpha_y \mathbf{L}_y - \beta \mathbf{I}] \mathbf{V}_d = \mathbf{V}_d \mathbf{A}_{dd} + \mathbf{V}_f \mathbf{A}_{fd}$$

$$\mathbf{V}_d^t \mathbf{V}_f = \mathbf{0}$$

$$\mathbf{V}_d^t [\alpha_x \mathbf{L}_x + \alpha_y \mathbf{L}_y - \beta \mathbf{I}] \mathbf{V}_d = \mathbf{A}_{dd}$$

$$\mathbf{A}_{dd} = \mathbf{P}_d \mathbf{\Sigma}_d \mathbf{P}_d^t$$

$$\boldsymbol{\varphi}_d = \mathbf{V}_d \mathbf{P}_d$$

$$\underbrace{\alpha_x \boldsymbol{\varphi}_d^t \mathbf{L}_x \boldsymbol{\varphi}_d}_{\text{non diag}} + \underbrace{\alpha_y \boldsymbol{\varphi}_d^t \mathbf{L}_y \boldsymbol{\varphi}_d}_{\text{non diag}} = \mathbf{\Sigma}_d + \beta \mathbf{I}_d$$

**MAIS**

$$\mathbf{\Sigma}_d \tilde{\simeq} \mathbf{\Sigma}$$

$$\text{eig}(\boldsymbol{\varphi}_d^t \mathbf{L}_{x,y} \boldsymbol{\varphi}_d) \tilde{\simeq} \text{eig}(\boldsymbol{\varphi}^t \mathbf{L}_{x,y} \boldsymbol{\varphi})$$

$d$  equations

$$\alpha_x \kappa_{pj}^2 + \alpha_y \gamma_{sj}^2 = -(\lambda_j + \beta)$$

## IN PRACTICE - With noise

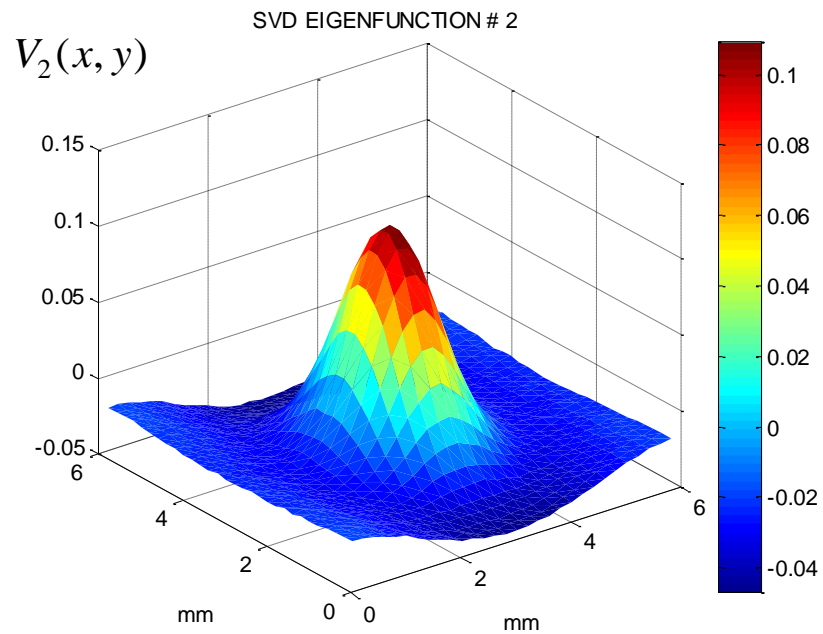
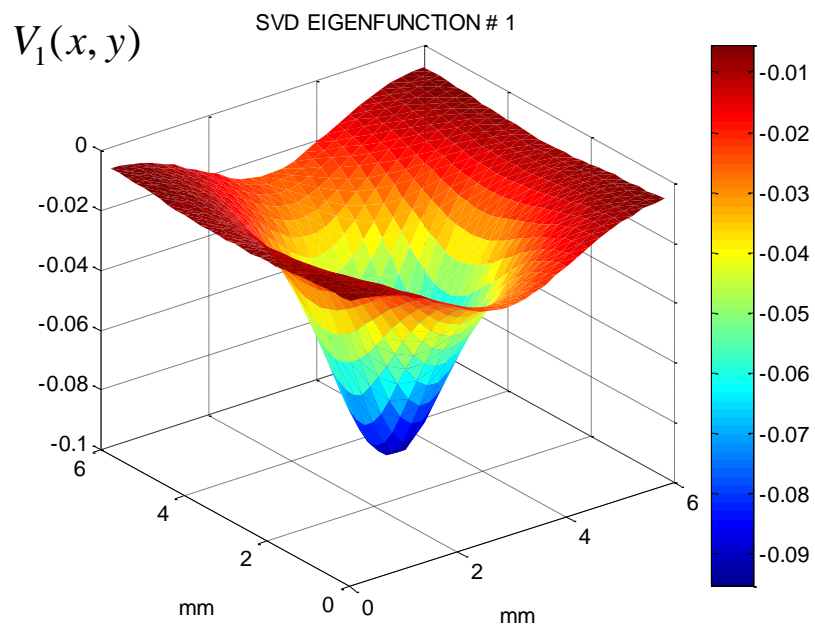
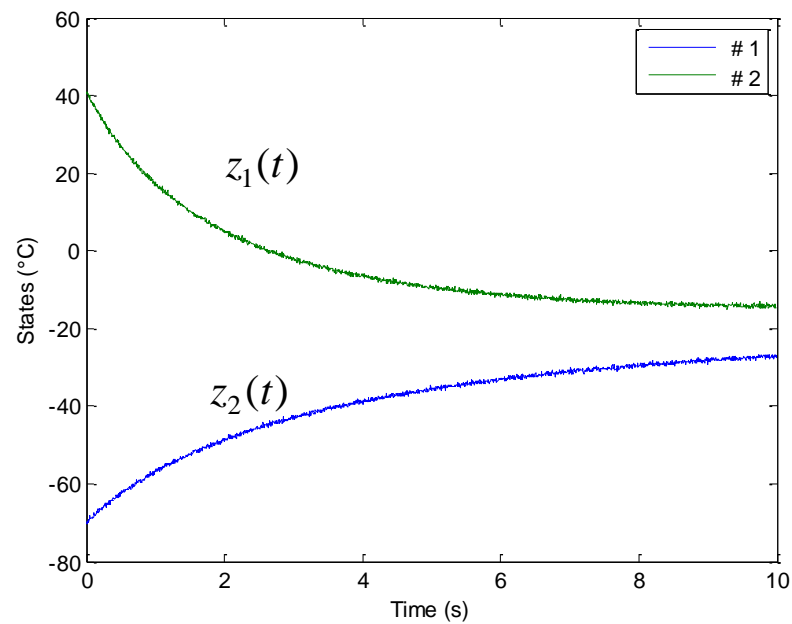
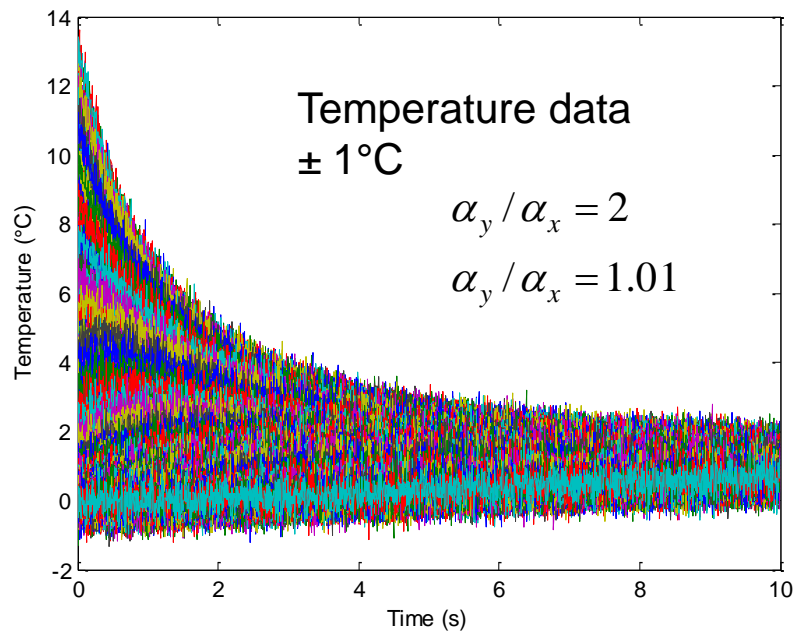
$$\tilde{\mathbf{T}}(t) \Rightarrow \mathbf{V}_d, \tilde{\sigma}_1^2, \tilde{\sigma}_2^2, \dots, \tilde{\sigma}_d^2, \tilde{z}_1(t), \tilde{z}_2(t), \dots, \tilde{z}_d(t)$$

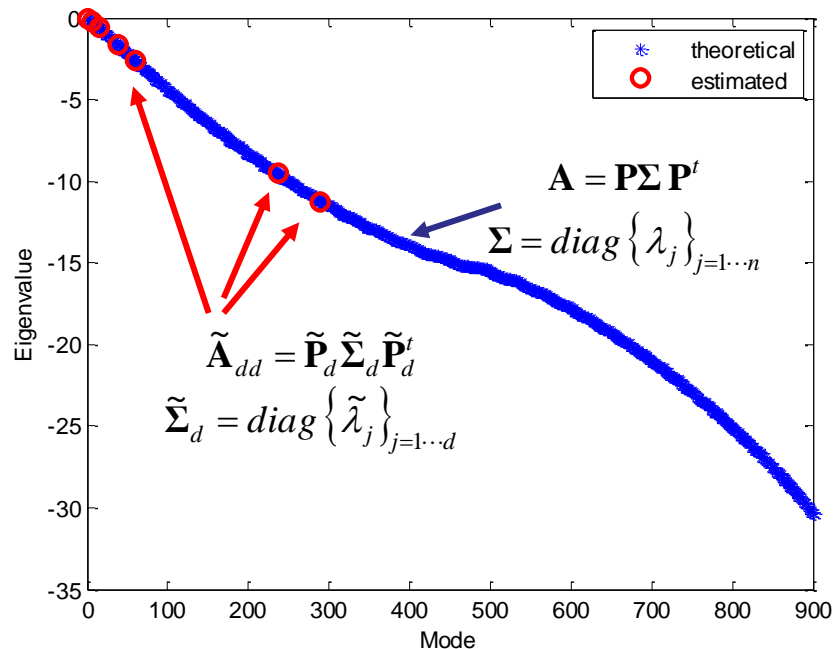
$$\tilde{a}_{mi} = \frac{\tilde{z}_m(t_f)\tilde{z}_i(t_f) - \tilde{z}_m(0)\tilde{z}_i(0)}{\tilde{\sigma}_m^2 + \tilde{\sigma}_i^2}; \quad m, i = 1, 2 \Rightarrow \tilde{\mathbf{A}}_{dd} \quad (d \times d)$$

$$\begin{array}{l} \tilde{\mathbf{A}}_{dd} = \tilde{\mathbf{P}}_d \tilde{\Sigma}_d \tilde{\mathbf{P}}_d^t \\ \tilde{\Phi}_d = \tilde{\mathbf{V}}_d \tilde{\mathbf{P}}_d \end{array} \xrightarrow[\begin{array}{l} \text{Closest analytical} \\ \text{OX \& OY eigenvalues} \end{array}]{\begin{array}{l} \text{Closest analytical} \\ \text{OX \& OY eigenvalues} \end{array}} \begin{array}{l} \kappa_{p1}, \kappa_{p2}, \dots, \kappa_{pd} \\ \gamma_{s1}, \gamma_{s2}, \dots, \gamma_{sd} \end{array}$$

$$\begin{array}{l} \text{eig}(\Phi_d^t \mathbf{L}_x \Phi_d) \rightarrow \tilde{\kappa}_{p1}, \tilde{\kappa}_{p2}, \dots, \tilde{\kappa}_{d1} \\ \text{eig}(\tilde{\Phi}_d^t \mathbf{L}_y \tilde{\Phi}_d) \rightarrow \tilde{\gamma}_{s1}, \tilde{\gamma}_{s2}, \dots, \tilde{\gamma}_{sd} \end{array}$$

$$\begin{array}{l} \alpha_x \kappa_{p1}^2 + \alpha_y \gamma_{s1}^2 = -(\tilde{\lambda}_1 + \hat{\beta}) \\ \alpha_x \kappa_{p2}^2 + \alpha_y \gamma_{s2}^2 = -(\tilde{\lambda}_2 + \hat{\beta}) \\ \dots\dots\dots \\ \alpha_x \kappa_{pd}^2 + \alpha_y \gamma_{sd}^2 = -(\tilde{\lambda}_d + \hat{\beta}) \end{array} \left\{ \begin{array}{l} \hat{\alpha}_x \\ \hat{\alpha}_y \end{array} \right.$$





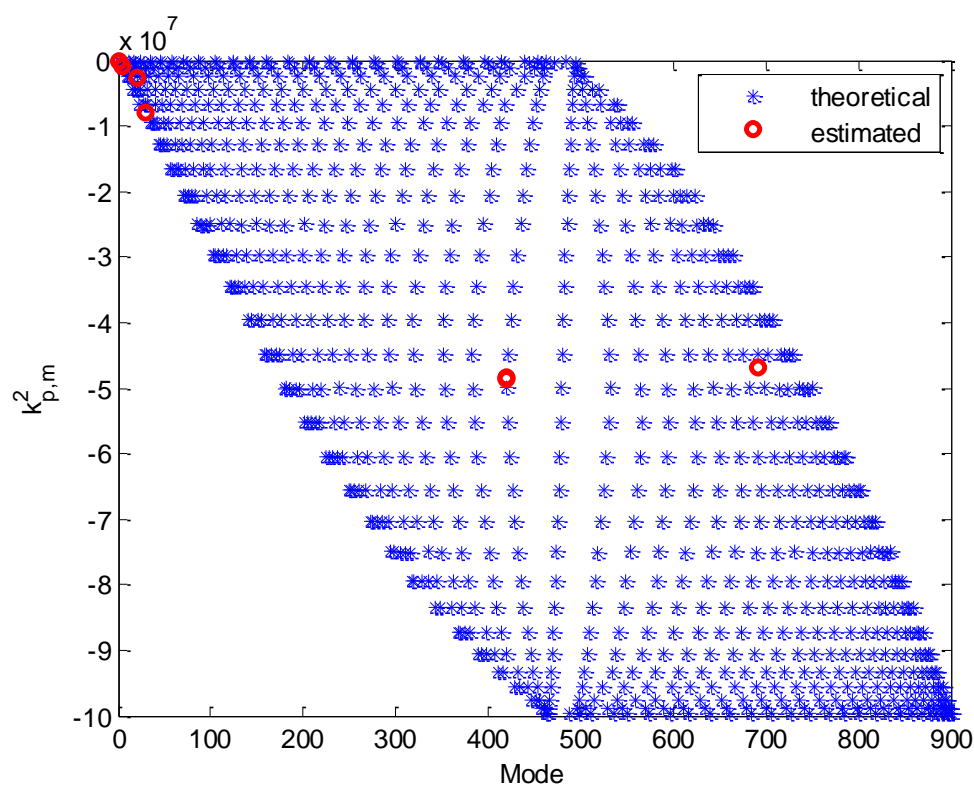
$\lambda_j$	$\tilde{\lambda}_j$
-0.0152	-0.0178
-0.1824	-0.1914
-0.5552	-0.5856
-1.6420	-1.6483
-2.5883	-2.5882
-9.5405	-9.5357
-11.2034	-11.2358

$\boldsymbol{\varphi}_d^t \mathbf{L}_x \boldsymbol{\varphi}_d$  non diagonal

-0.0041	0.0040	0.0074	0.0108	0.0307	0.0125	0.0002
0.0040	-0.0813	-0.0284	-0.0014	-0.0814	0.0102	-0.0241
0.0074	-0.0284	-0.3358	0.1455	-0.1605	0.2043	-0.1677
0.0108	-0.0014	0.1455	-1.8630	-1.6206	-0.7192	0.3088
0.0307	-0.0814	-0.1605	-1.6206	-4.0645	0.3012	-0.4070
0.0125	0.0102	0.2043	-0.7192	0.3012	-4.5169	-0.2379
0.0002	-0.0241	-0.1677	0.3088	-0.4070	-0.2379	-4.8431

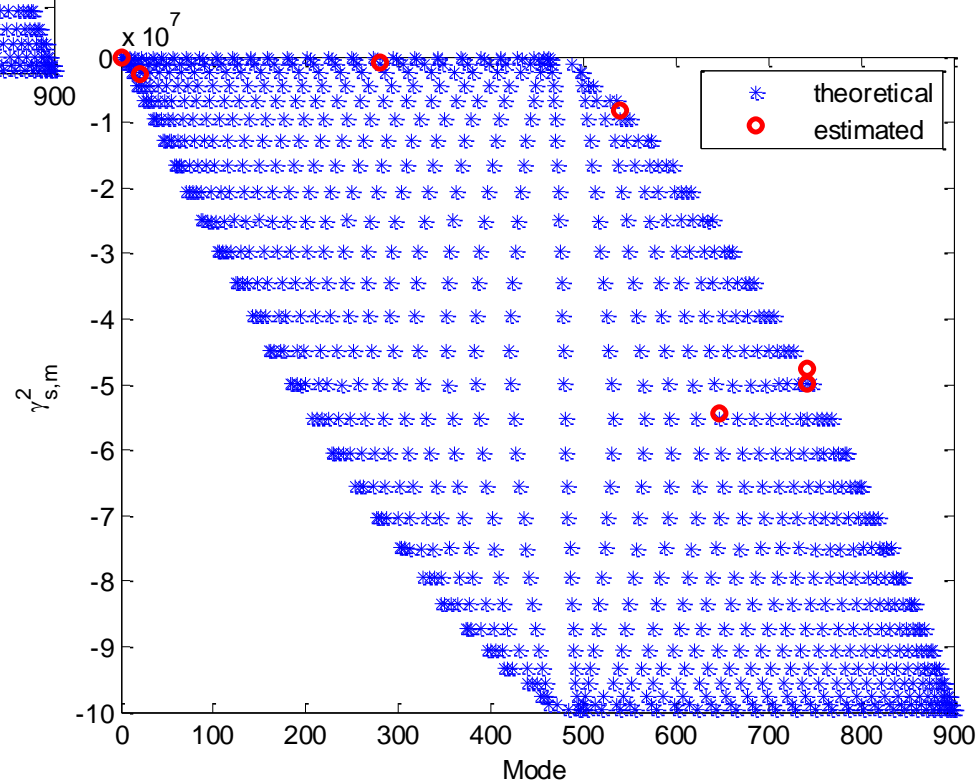
$k_j^2$	$\tilde{k}_j^2$
-0.6699	-0.7892
-0.2447	-0.2697
-0.0000	-0.0036
-0.1093	-0.0771
-4.4774	-4.6858
-5.0000	-4.8604
-5.0000	-4.8391

$\text{eig}(\boldsymbol{\varphi}_d^t \mathbf{L}_x \boldsymbol{\varphi}_d)$



$$\tilde{\kappa}_{p,m} = \tilde{p} \pi / L \Rightarrow \tilde{p} \Rightarrow p \Rightarrow \kappa_{p,m} = p \pi / L$$

$$\tilde{\gamma}_{s,m} = \tilde{s} \pi / L \Rightarrow \tilde{s} \Rightarrow s \Rightarrow \gamma_{s,m} = s \pi / L$$



$$\alpha_y / \alpha_x = 2$$

Noise amplitude $\pm 1.00\text{ }^{\circ}\text{C}$	$\hat{\alpha}_x$ ( $\times 10^{-6} m^2 s^{-1}$ )	$\left  \frac{\alpha_x - \hat{\alpha}_x}{\alpha_x} \right  \times 100$	$\hat{\alpha}_y$ ( $\times 10^{-6} m^2 s^{-1}$ )	$\left  \frac{\alpha_y - \hat{\alpha}_y}{\alpha_y} \right  \times 100$
SVD	0.1468 ( $\pm 0.018$ )	3.13	0.3091 ( $\pm 0.028$ )	2.00
CI-SVD	0.1468 ( $\pm 0.015$ )	3.12	0.3091 ( $\pm 0.025$ )	2.00
<b>Modal-SVD</b>	<b>0.1515</b> <b>(<math>\pm 0.0012</math>)</b>	<b>0.009</b>	<b>0.3030</b> <b>(<math>\pm 0.0026</math>)</b>	<b>0.0013</b>

Noise amplitude $\pm 1.00\text{ }^{\circ}\text{C}$	$\hat{\alpha}_x$ ( $\times 10^{-6} m^2 s^{-1}$ )	$\left  \frac{\alpha_x - \hat{\alpha}_x}{\alpha_x} \right  \times 100$	$\hat{\alpha}_y$ ( $\times 10^{-6} m^2 s^{-1}$ )	$\left  \frac{\alpha_y - \hat{\alpha}_y}{\alpha_y} \right  \times 100$
SVD	0.0286 ( $\pm 1.2$ )	81.12	0.2760 ( $\pm 1.0$ )	80.37
CI-SVD	- 0.0036 ( $\pm 1.0$ )	102.3	0.3085 ( $\pm 1.0$ )	101.6
<b>Modal-SVD</b>	<b>0.1524</b> <b>(<math>\pm 0.0014</math>)</b>	<b>0.58</b>	<b>0.1539</b> <b>(<math>\pm 0.0013</math>)</b>	<b>0.585</b>

$$\alpha_y / \alpha_x = 1.01$$

# ESTIMATIONS IMPROVEMENT

## Modal approach

$$\phi_j(x, y) = (2/L) \cos(\kappa_p x) \cos(\gamma_s y)$$

$$\kappa_p = p\pi/L; \gamma_s = s\pi/L$$

$$T(x, y, t) = \sum_{j=1}^{\infty} \phi_j(x, y) \eta_j(t)$$

$$\eta_j(t) = \eta_j(0) \exp(-\lambda_j t)$$

$$\alpha_x \kappa_{pj}^2 + \alpha_y \gamma_{sj}^2 = -(\lambda_j + \beta)$$

$$\tilde{\mathbf{\eta}}(t) = \boldsymbol{\Phi}^t \tilde{\mathbf{T}}(t)$$

$$\text{diag} \left[ \int_{t=0}^{t_{fin}} \tilde{\mathbf{\eta}}(t) \tilde{\mathbf{\eta}}^t(t) dt \right]$$

Selection of 3 states  
Those with greater energy

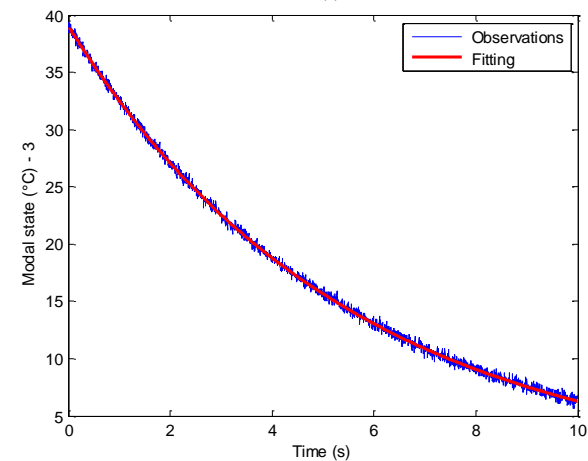
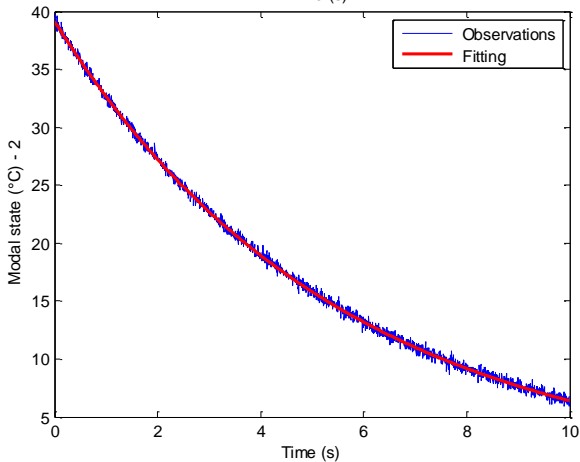
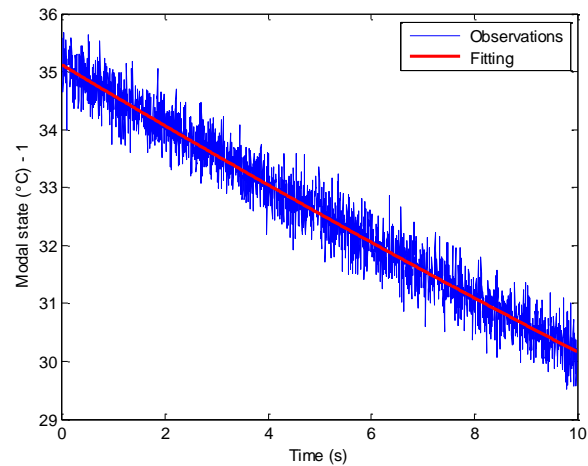
$$\tilde{\eta}_j(t) \quad j = a, b, c \Rightarrow \kappa_{pj}^2, \gamma_{sj}^2$$

$$\alpha_x \kappa_{pj}^2 + \alpha_y \gamma_{sj}^2 = -(\tilde{\lambda}_j + \hat{\beta})$$

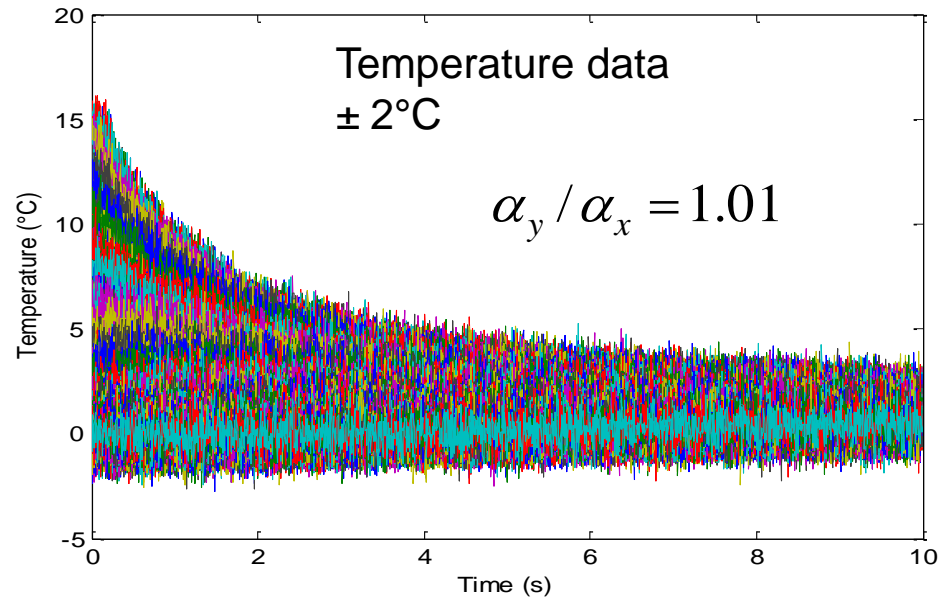
Eigenvalues estimation  
(minimum least squares)

$$\eta_j(t) = \eta_j(0) \exp(-\lambda_j t)$$





$\lambda_j$	$\tilde{\lambda}_j$	$p$	$s$
-0.0152	-0.0151	0	0
-0.1807	-0.1808	2	0
-0.1824	-0.1827	0	2



$$\hat{\alpha}_x = 0.1518 \pm 0.0009 \text{ mm}^2/\text{s} \text{ (bias: 0.20\%)}$$

$$\hat{\alpha}_y = 0.1534 \pm 0.0008 \text{ mm}^2/\text{s} \text{ (bias: 0.26\%)}$$

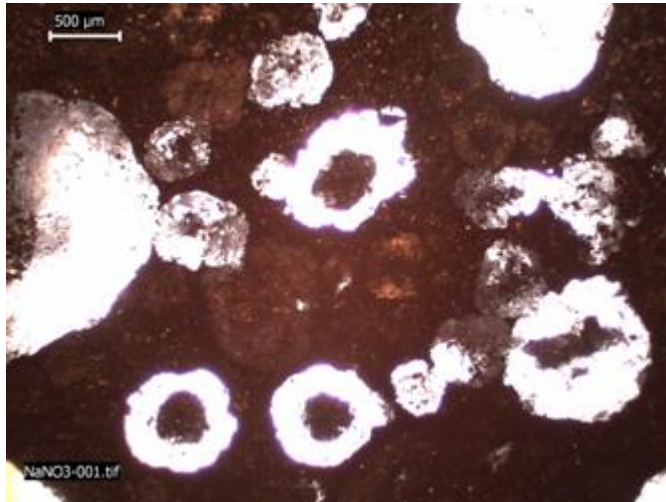
**MODAL**

$$\hat{\alpha}_x = 0.1517 \pm 0.0105 \text{ mm}^2/\text{s} \text{ (bias: 0.13\%)}$$

$$\hat{\alpha}_y = 0.1535 \pm 0.0029 \text{ mm}^2/\text{s} \text{ (bias: 0.32\%)}$$

**MODAL  
SVD**

# Heterogeneous materials



Adiabatic boundary conditions

$p$  non overlapping homogeneous phases paving the domain

Within the phases

$$\frac{\partial T(\mathbf{x}, t)}{\partial t} = \alpha_i \nabla^2 T(\mathbf{x}, t) - \beta_i T(\mathbf{x}, t)$$

At the interfaces

$$-k_i \nabla T(\mathbf{x}, t) \cdot \mathbf{n}_{ij} = -h_{ij} (T(\mathbf{x}, t)|^i - T(\mathbf{x}, t)|^j)$$

$$-k_j \nabla T(\mathbf{x}, t) \cdot \mathbf{n}_{ji} = -h_{ij} (T(\mathbf{x}, t)|^j - T(\mathbf{x}, t)|^i)$$

**Microstructure**  
Phases discrimination  
Interfaces location



**Thermal diffusivity  
of the phases**

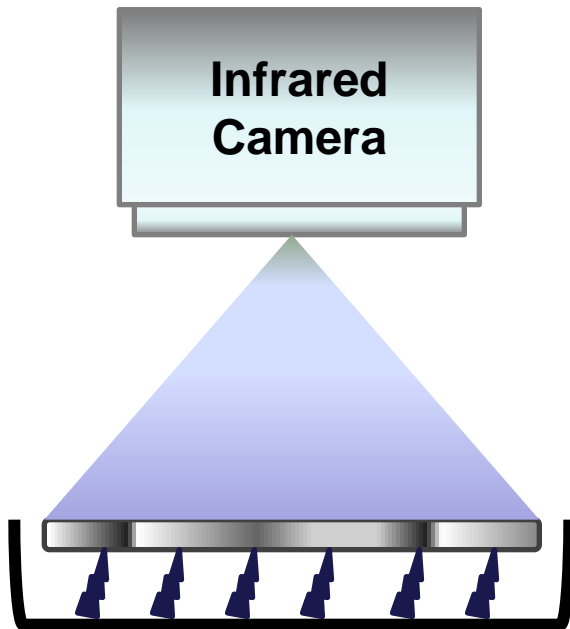


**Thermal resistance  
at the interfaces**

# MICROSTRUCTURE RETRIEVAL

## Phases discrimination – Interfaces location

Applying a **uniform heat flux** on the back side of the sample during a **very short time** & recording the thermal behavior of the plate via an IR camera



Negligible/limited heat diffusion between adjacent pixels

The thermal behavior of a pixel is determined by its thermal capacity  
All the pixels belonging to the same phase behave in the same way

$$\forall (x, y) \in \Omega_i$$

$$T_i(t) = (\varphi / \beta_i)(1 - \exp(-\beta_i t))$$

$$\frac{\partial T(x, y, t)}{\partial t} = \alpha_i \nabla^2 T(x, y, t) - \beta_i T(x, y, t) + \varphi$$

+ Robin conditions at the interfaces  
+ Adiabatic boundary conditions

$$W(\mathbf{x}, \mathbf{x}') = \sum_{m=1}^{\infty} \sigma_m^2 V_m(\mathbf{x}) V_m(\mathbf{x}')$$

$$\forall t, T(\mathbf{x}, t) = \sum_{m=1}^{\infty} V_m(\mathbf{x}) z_m(t)$$

**SVD – Noise, parsimony**  
**Likeness**

**Number of phases**

Rank of the energy matrix W =  
Number of phases

**Discontinuity of the eigenfunctions at the interfaces**

$$\forall (x, y) \& (x', y') \in \Omega_i, \forall m \Rightarrow V_m(x, y) = V_m(x', y')$$

$$\forall (x, y) \in \Omega_i \& (x', y') \in \Omega_j, \forall m \Rightarrow V_m(x, y) \neq V_m(x', y')$$

**Eigenfunctions sign**

→ **Criteria for phases discrimination**

$$\forall m > 1 \quad \langle V_m(x, y) \rangle_{\Omega} = 0$$

$$\forall (x, y) \in \Omega_i \& (x', y') \in \Omega_j, \exists m / V_m(x, y) V_m(x', y') < 0$$

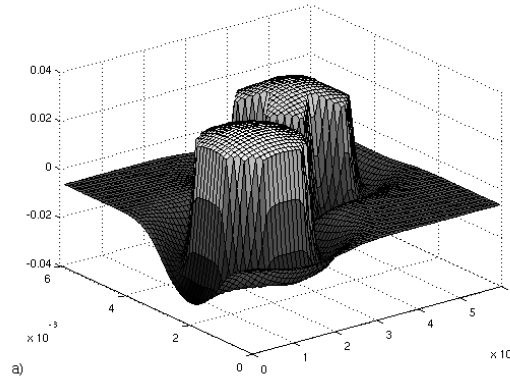
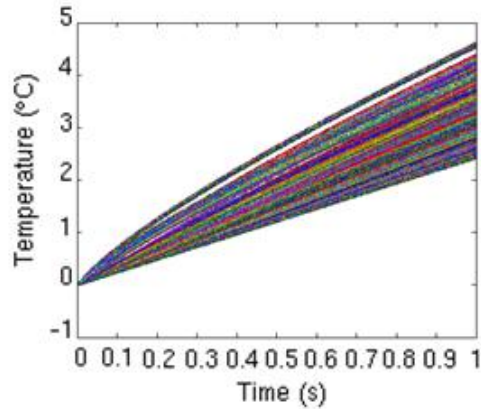
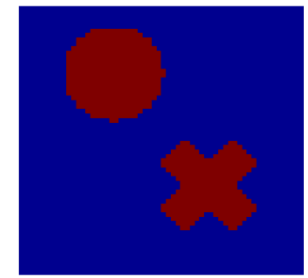
**IDEAL CASE**

With infinite thermal  
resistance at the interfaces

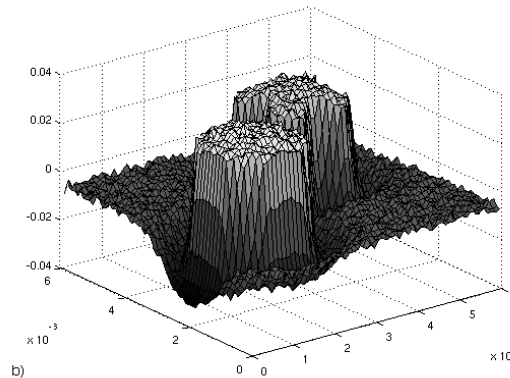
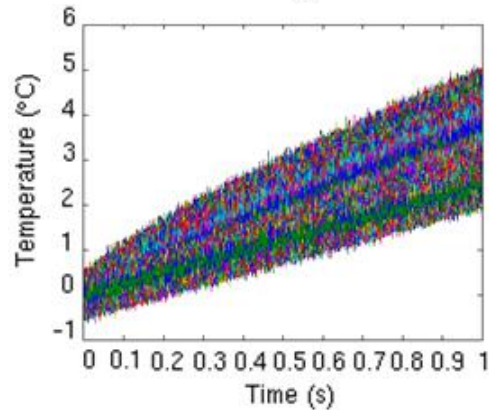
$$\forall (x, y) \in \Omega_i$$

$$T_i(t) = (\varphi / \beta_i)(1 - \exp(-\beta_i t))$$

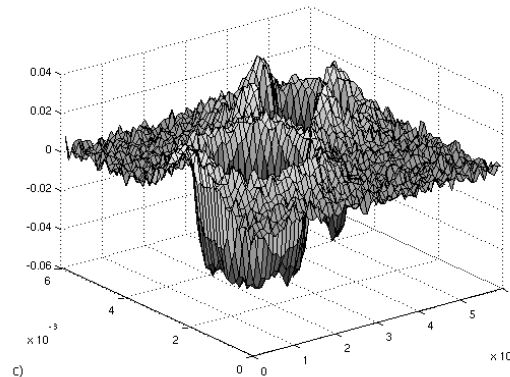
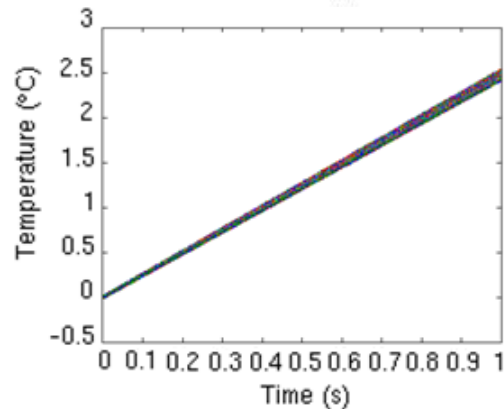
# NUMERICAL TEST



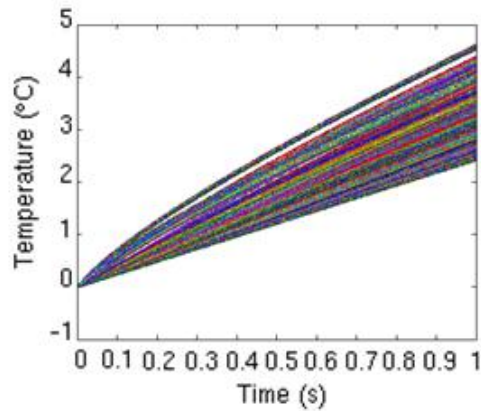
**High contrast** between phases in terms of thermal properties ( $\alpha_b/\alpha_r = 134.7$ )  
**High quality** measurements ( $\pm 0.02^\circ\text{C}$ )



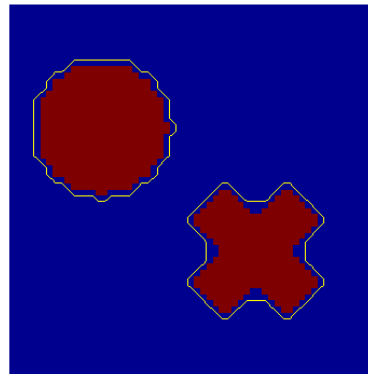
**High contrast** between phases in terms of thermal properties ( $\alpha_b/\alpha_r = 134.7$ )  
**Bad quality** measurements ( $\pm 0.5^\circ\text{C}$ )



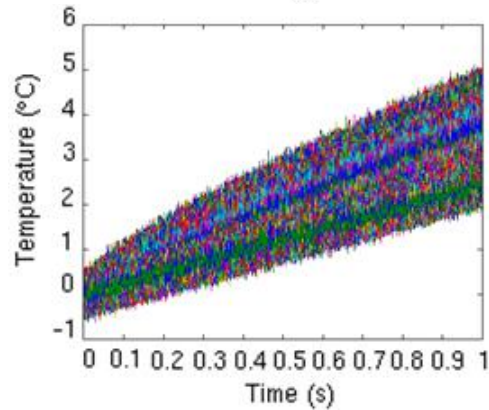
**Very low contrast** between phases in terms of thermal properties ( $\alpha_b/\alpha_r = 1.05$ )  
**High quality** measurements ( $\pm 0.02^\circ\text{C}$ )



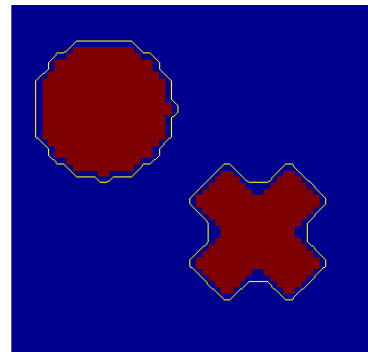
a)



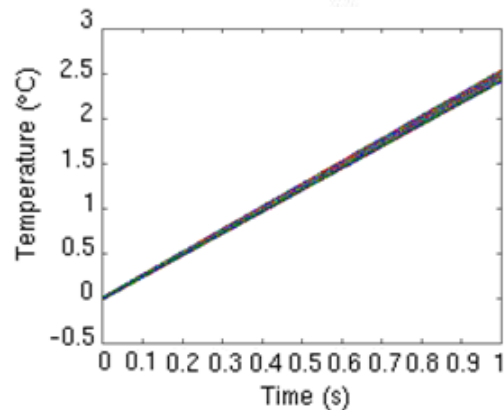
**High contrast** between phases in terms of thermal properties ( $\alpha_b/\alpha_r = 134.7$ )  
**High quality** measurements ( $\pm 0.02^\circ\text{C}$ )



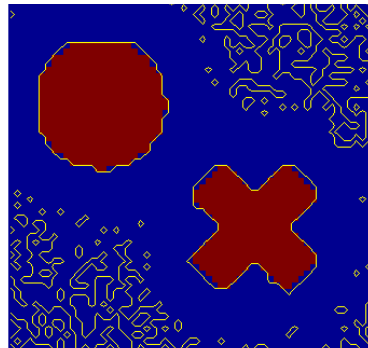
b)



**High contrast** between phases in terms of thermal properties ( $\alpha_b/\alpha_r = 134.7$ )  
**Bad quality** measurements ( $\pm 0.5^\circ\text{C}$ )



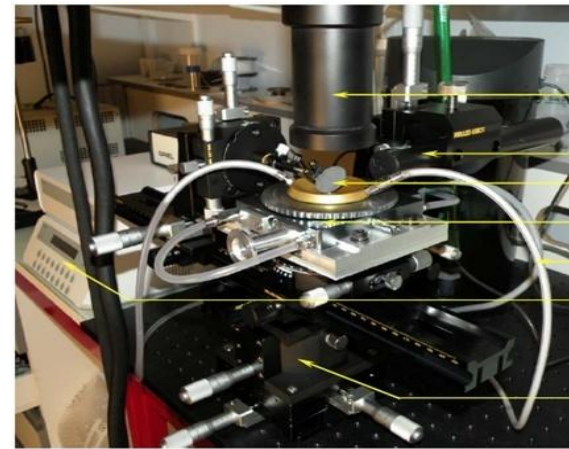
c)



**Very low contrast** between phases in terms of thermal properties ( $\alpha_b/\alpha_r = 1.05$ )  
**High quality** measurements ( $\pm 0.02^\circ\text{C}$ )



# EXPERIMENTAL TEST

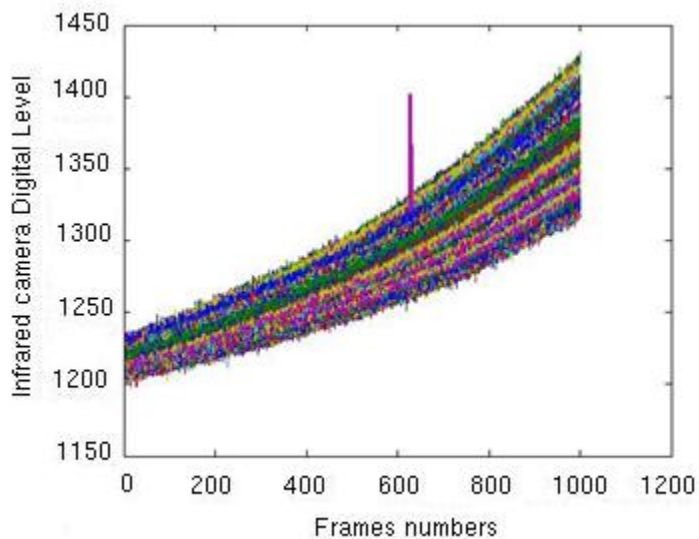


Microscope lens

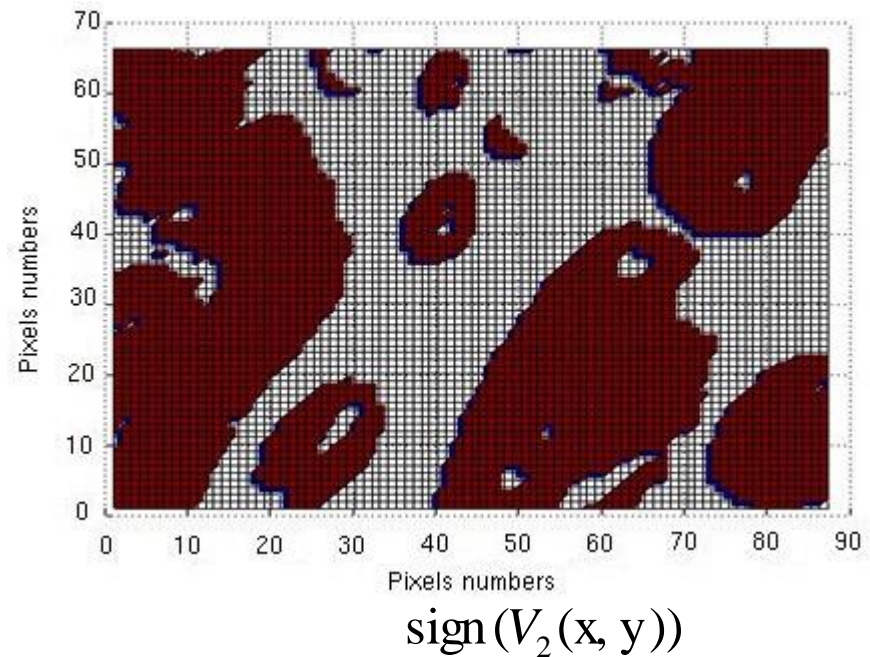
Furnace

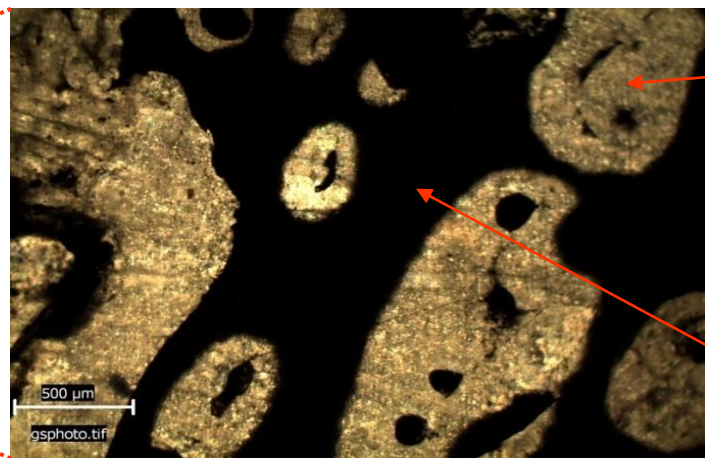
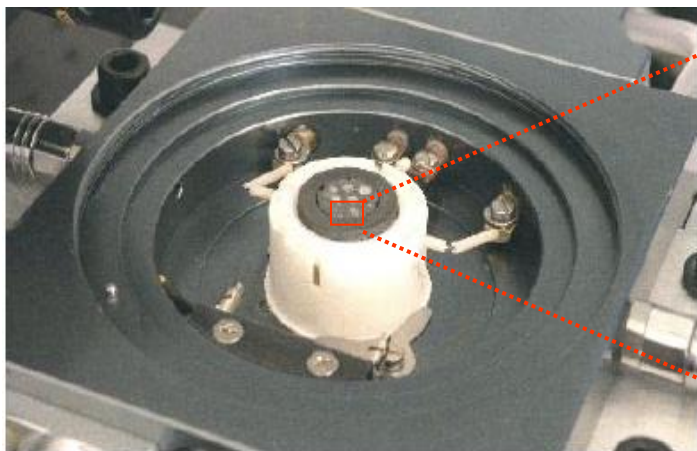
Furnace programmer

x-y-z-translation system



Thermal response

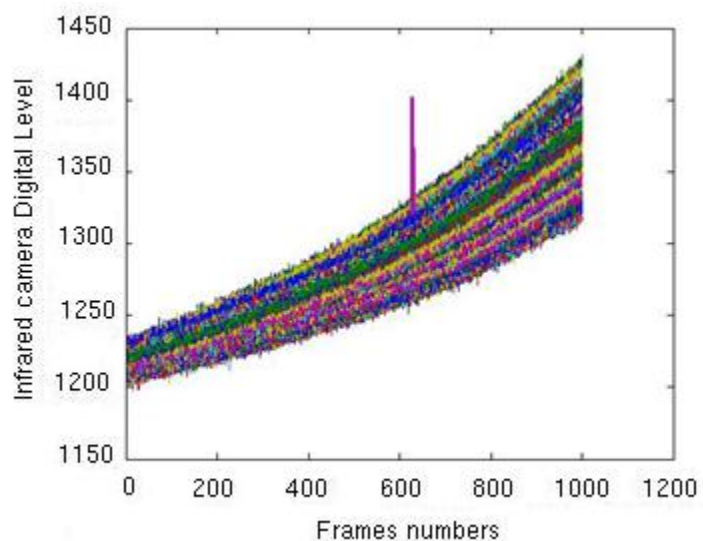




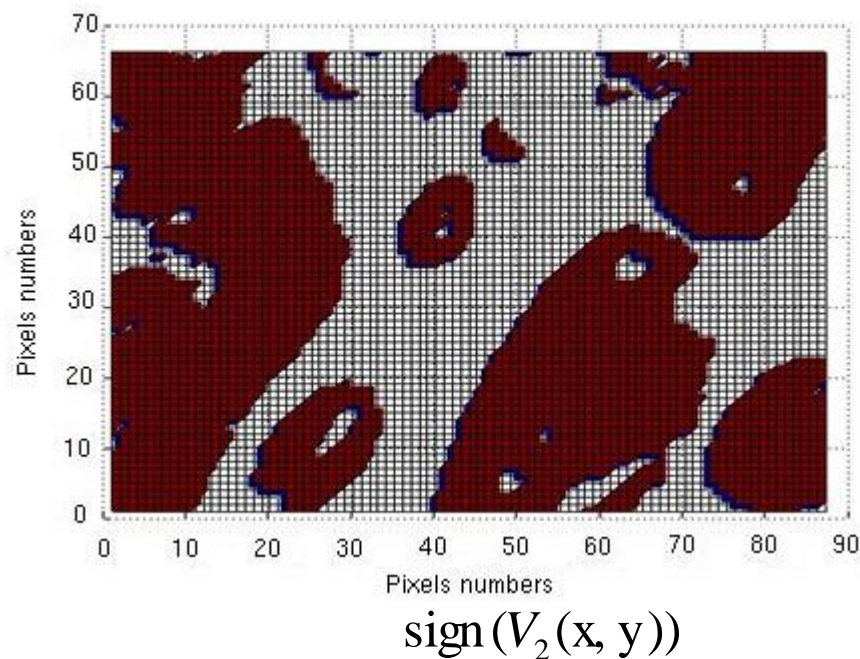
salt

carbon

Optical microscopic picture

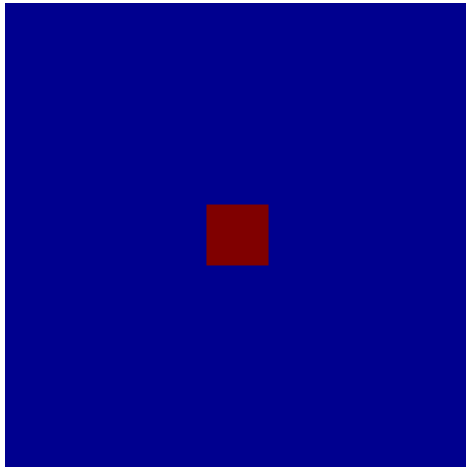


Thermal response

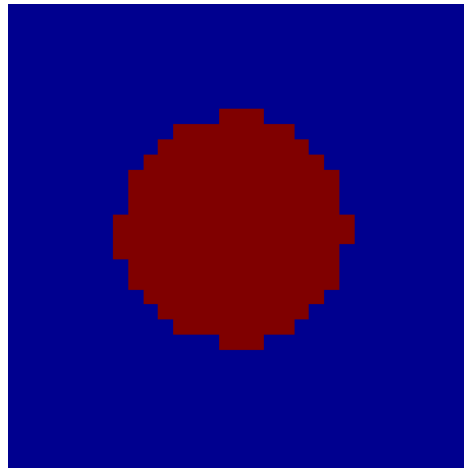




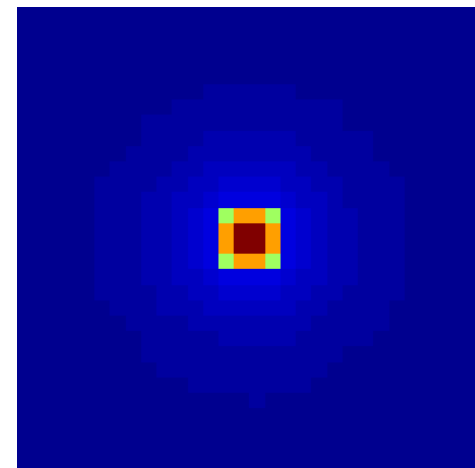
... but



$\text{sgn}(V_2(x, y))$



$V_2(x, y)$



$$u(x, y, t) = \int_0^t T(x, y, \tau) d\tau$$

$$u(x, y, t) = \sum_{m=1}^{\infty} V_m(x, y) z_m(t)$$



$$\Omega_i : f_m(x, y) = \alpha_i \nabla^2 V_m(x, y, t) - \beta_i V_m(x, y, t)$$

$$\Gamma : \begin{cases} k_i \partial_n V_m(x, y, t)|_i - k_j \partial_n V_m(x, y, t)|_j = 0 \\ V_m(x, y, t)|_i = V_m(x, y, t)|_j \end{cases}$$

$$\text{with } f_m(x, y) = (1/\sigma_m^2) [\langle T, z_m \rangle_t - \phi \langle t, z_m \rangle_t]$$

**Level-set method**

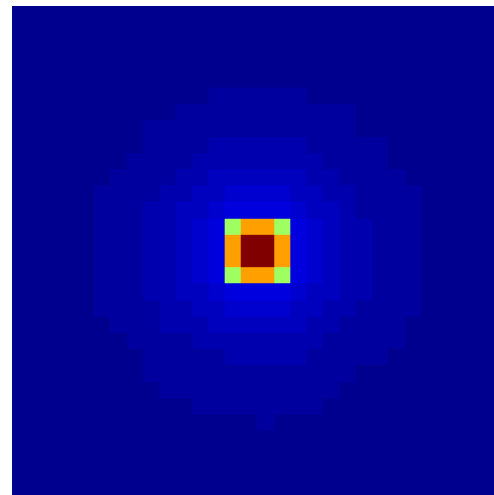
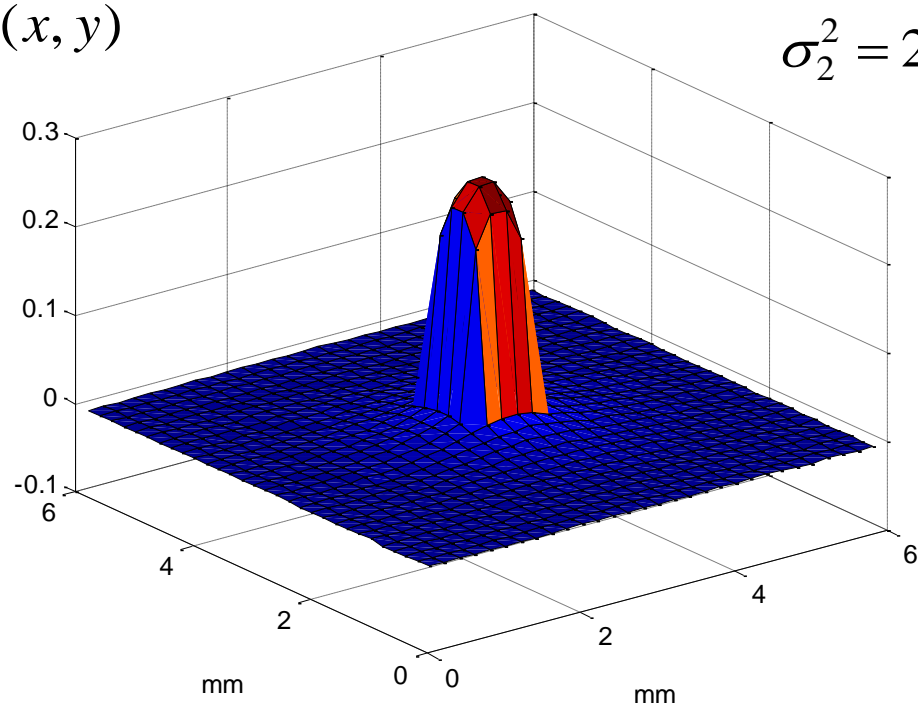
Look for  $\Gamma$  that minimizes the cost function

$$J = \int_{\Omega} (\tilde{f}_m(x, y) - f_m(x, y))^2 dx dy$$

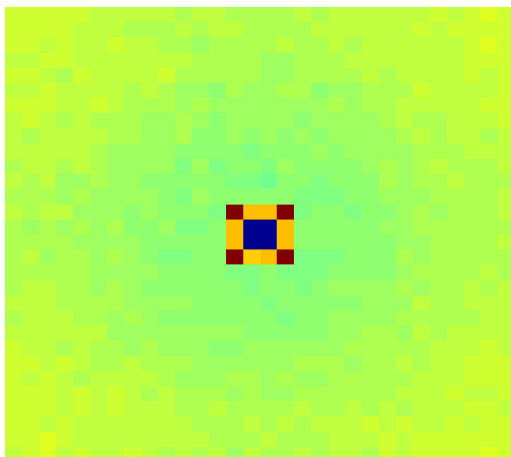
$V_2(x, y)$

EIGENFUNCTION 2

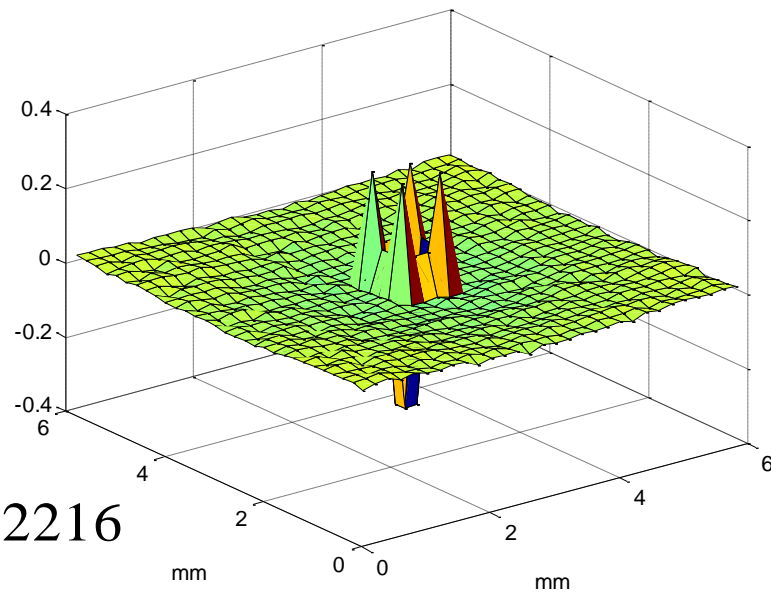
$\sigma_2^2 = 230.74$



$V_3(x, y)$



EIGENFUNCTION 3



$\sigma_3^2 = 2.2216$

$$\frac{\partial T(x, y, t)}{\partial t} = \alpha_i \nabla^2 T(x, y, t) - \beta_i T(x, y, t)$$

+ Robin & adiabatic boundary conditions

$$T(x, y, t) = \sum_{m=1}^{\infty} V_m(x, y) z_m(t)$$

$$\langle V_k, V_m \rangle_{\Omega} \equiv \int_{\Omega} V_k(x) V_m(x) dx = \delta_{km}$$

$$\langle z_m(t), z_k(t) \rangle_t \equiv \int_t z_m(t) z_k(t) dt = \delta_{mk} \sigma_m^2$$

$$\langle \langle \circ, V_k \rangle_{\Omega}, z_k(t) \rangle_t$$

## DIFFUSIVITIES ESTIMATION SVD-based method

Integration  
over  $\Omega$

$$\sum_{i=1}^p \frac{\varepsilon_i}{\beta_i} \frac{d \langle T \rangle_{\Omega_i}}{dt} = - \langle T \rangle_{\Omega}$$

**ESTIMATION  $\beta_1$  &  $\beta_2$**   
linear least squares  
methods

$$i = 1, 2, 3, \dots; \quad k = i, i+1, i+2, \dots$$

$$y_k = \sum_{i=1}^p \alpha_i \langle \nabla^2 V_k(x, y), V_k(x, y) \rangle_{\Omega_i} - \sum_{i=1}^p \beta_i \langle V_k(x, y), V_k(x, y) \rangle_{\Omega_i}$$

$$y_k = \frac{z_k^2(t_f) - z_k^2(0)}{2\sigma_k^2}$$

No knowledge about the  
thermal parameters at the  
interfaces is required !!

Noise & bias considerations

→ Diffusivities estimated by

$$\begin{bmatrix} \hat{\alpha}_1 \\ \vdots \\ \hat{\alpha}_p \end{bmatrix} = \mathbf{M}^{-1} \mathbf{y}$$

$$\mathbf{y} = \begin{bmatrix} \Delta \tilde{z}_1^2 / \tilde{\sigma}_1^2 + \sum_{i=1}^2 \hat{\beta}_i \langle V_1(\mathbf{x}), V_1(\mathbf{x}) \rangle_{\Omega_i} \\ \Delta \tilde{z}_2^2 / \tilde{\sigma}_2^2 + \sum_{i=1}^2 \hat{\beta}_i \langle V_2(\mathbf{x}), V_2(\mathbf{x}) \rangle_{\Omega_i} \\ \dots \\ \Delta \tilde{z}_p^2 / \tilde{\sigma}_p^2 + \sum_{i=1}^2 \hat{\beta}_i \langle V_p(\mathbf{x}), V_p(\mathbf{x}) \rangle_{\Omega_i} \end{bmatrix} \quad \Delta \tilde{z}_i^2 = \frac{1}{2} \tilde{z}_i^2 \Big|_{t=0}^{t_f}$$

$$\mathbf{M} = \begin{bmatrix} \langle \nabla^2 V_1(\mathbf{x}), V_1(\mathbf{x}) \rangle_{\Omega_1} & \dots & \langle \nabla^2 V_1(\mathbf{x}), V_1(\mathbf{x}) \rangle_{\Omega_p} \\ \langle \nabla^2 V_2(\mathbf{x}), V_2(\mathbf{x}) \rangle_{\Omega_1} & \dots & \langle \nabla^2 V_2(\mathbf{x}), V_2(\mathbf{x}) \rangle_{\Omega_p} \\ \dots & \dots & \dots \\ \langle \nabla^2 V_p(\mathbf{x}), V_p(\mathbf{x}) \rangle_{\Omega_1} & \dots & \langle \nabla^2 V_p(\mathbf{x}), V_p(\mathbf{x}) \rangle_{\Omega_p} \end{bmatrix}$$

## ESTIMATIONS BY Cumulative integral-SVD method

$$u(x, y, t) = \int_0^t T(x, y, \tau) d\tau$$

$$u(x, y, t) = \sum_{m=1}^{\infty} V_m(x, y) z_m(t)$$

$$\Delta T(x, y, t) = \sum_{m=1}^{\infty} V_m(x, y) \eta_m(t)$$

$$\mathbf{y} = \begin{bmatrix} \langle \eta_1, z_1 \rangle_t / \tilde{\sigma}_1^2 + \sum_{i=1}^2 \hat{\beta}_i \langle V_1(\mathbf{x}), V_1(\mathbf{x}) \rangle_{\Omega_i} \\ \langle \eta_2, z_2 \rangle_t / \tilde{\sigma}_2^2 + \sum_{i=1}^2 \hat{\beta}_i \langle V_2(\mathbf{x}), V_2(\mathbf{x}) \rangle_{\Omega_i} \\ \dots \\ \langle \eta_p, z_p \rangle_t / \tilde{\sigma}_p^2 + \sum_{i=1}^2 \hat{\beta}_i \langle V_p(\mathbf{x}), V_p(\mathbf{x}) \rangle_{\Omega_i} \end{bmatrix}$$

# ESTIMATIONS BY Modal-SVD method

$$\alpha_i \begin{bmatrix} \nabla^2 V_1(x, y) \\ \nabla^2 V_2(x, y) \\ \vdots \end{bmatrix} - \beta_i \begin{bmatrix} V_1(x, y) \\ V_2(x, y) \\ \vdots \end{bmatrix} = \mathbf{A} \begin{bmatrix} V_1(x, y) \\ V_2(x, y) \\ \vdots \end{bmatrix}$$

+ Robin conditions & adiabatic BC

$$\begin{bmatrix} \phi_1(x, y) \\ \phi_2(x, y) \\ \vdots \end{bmatrix} = \mathbf{P}^t \begin{bmatrix} V_1(x, y) \\ V_2(x, y) \\ \vdots \end{bmatrix}$$

$$\mathbf{A} = \{a_{mi}\}$$

$$a_{mj} = \frac{1}{\sigma_j^2} \left\langle \dot{z}_m(t) z_j(t) \right\rangle_t$$

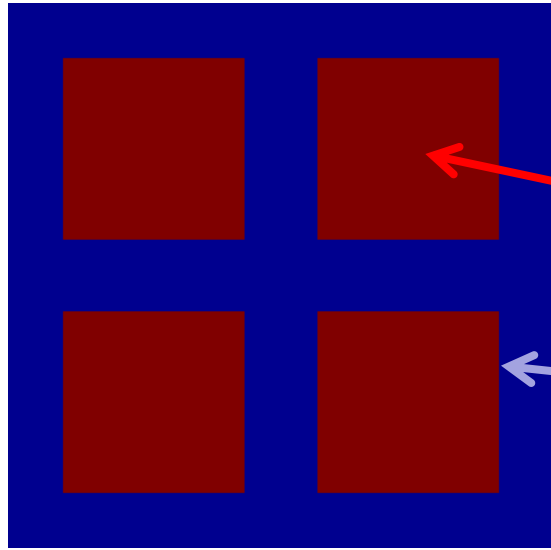
$$\mathbf{Q}^t \mathbf{A} \mathbf{P} = \mathbf{\Sigma}$$

$$\mathbf{P}^t \mathbf{Q} = \mathbf{I}; \quad \mathbf{Q}^t \mathbf{P} = \mathbf{I}; \quad \mathbf{\Sigma} = \text{diag}\{\lambda_m\}$$

Set of independent PDE

$$\begin{aligned} \alpha_i \nabla^2 \phi_m(x, y) - \beta_i \phi_m(x, y) &= \lambda_m \phi_m(x, y) & (x, y) \in \Omega_i \\ \nabla \phi_m(x, y) \mathbf{n} &= 0 & (x, y) \in \partial\Omega_i \\ k_i \nabla \phi_m(x, y) \mathbf{n} &= h(\phi_m(x, y)|_i - \phi_m(x, y)|_j) & (x, y) \in \partial\Omega_{ij} \end{aligned}$$

Eigenfunctions/Eigenvalues  
problem associated to the  
thermal equations



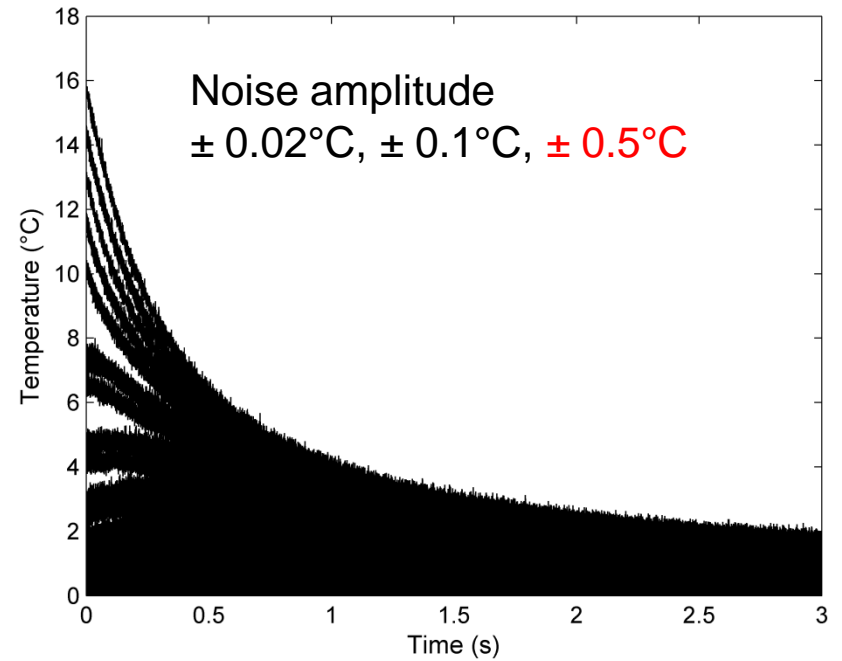
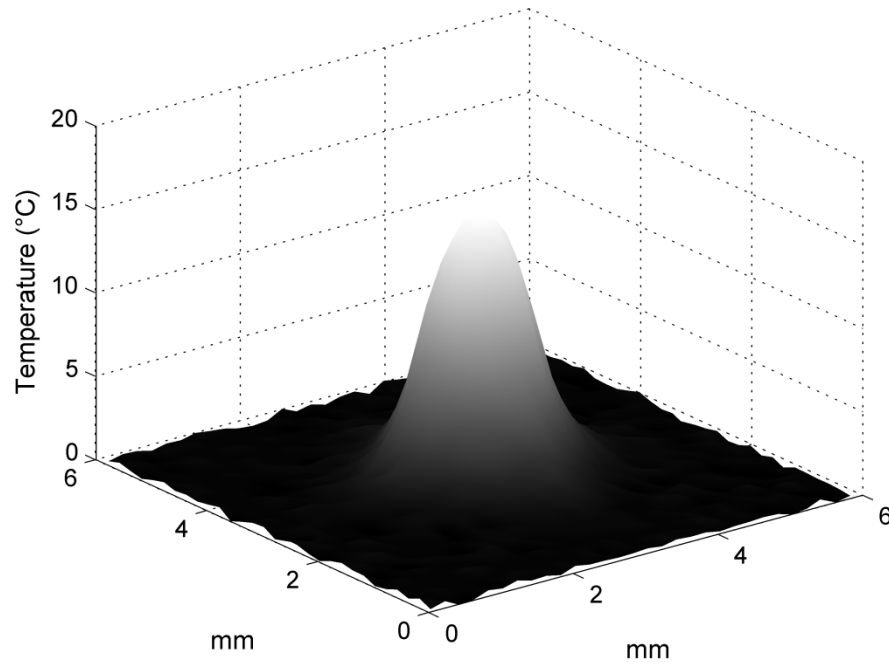
## NUMERICAL TEST SVD-based method

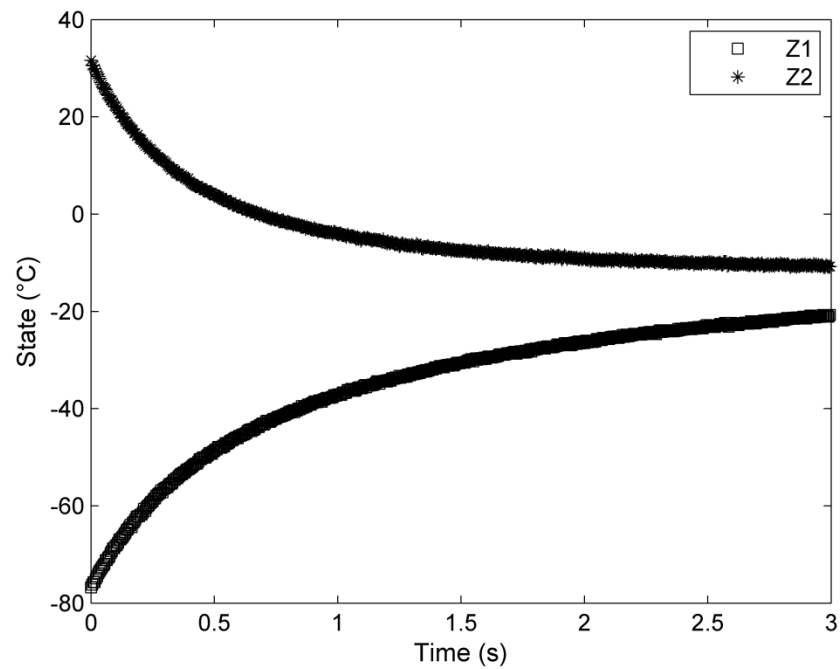
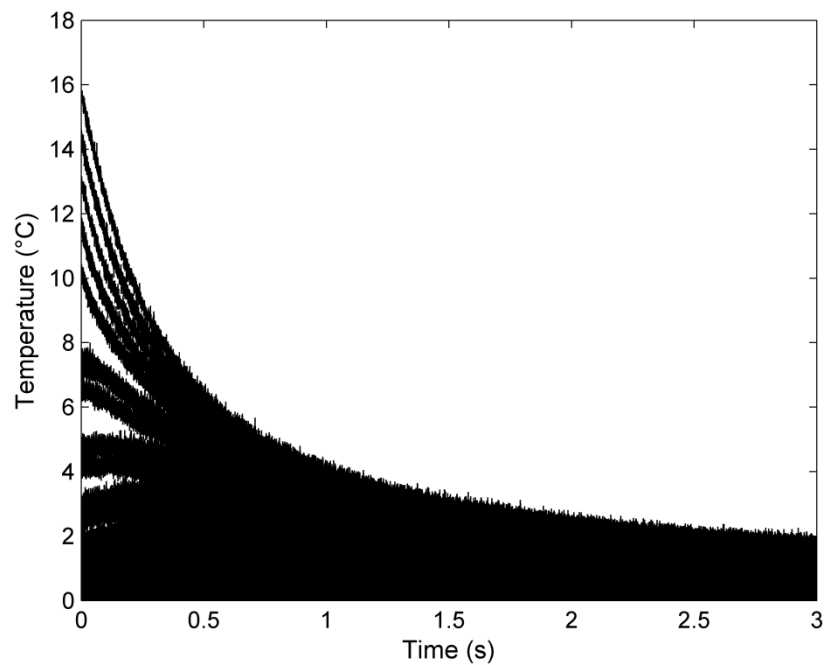
$$\alpha_1 = 1.5152 \times 10^{-7} \text{ m}^2 \cdot \text{s}^{-1}$$

$$\beta_1 = 0.0061 \text{ s}^{-1}$$

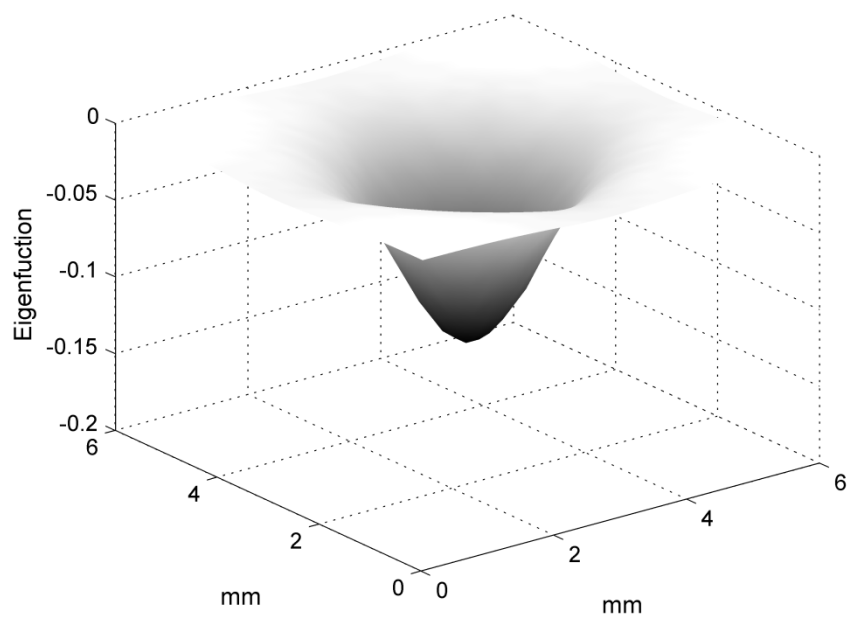
$$\alpha_2 = 5.0505 \times 10^{-7} \text{ m}^2 \cdot \text{s}^{-1}$$

$$\beta_2 = 0.0202 \text{ s}^{-1}$$





EIGENFUNCTION # 1



EIGENFUNCTION # 2

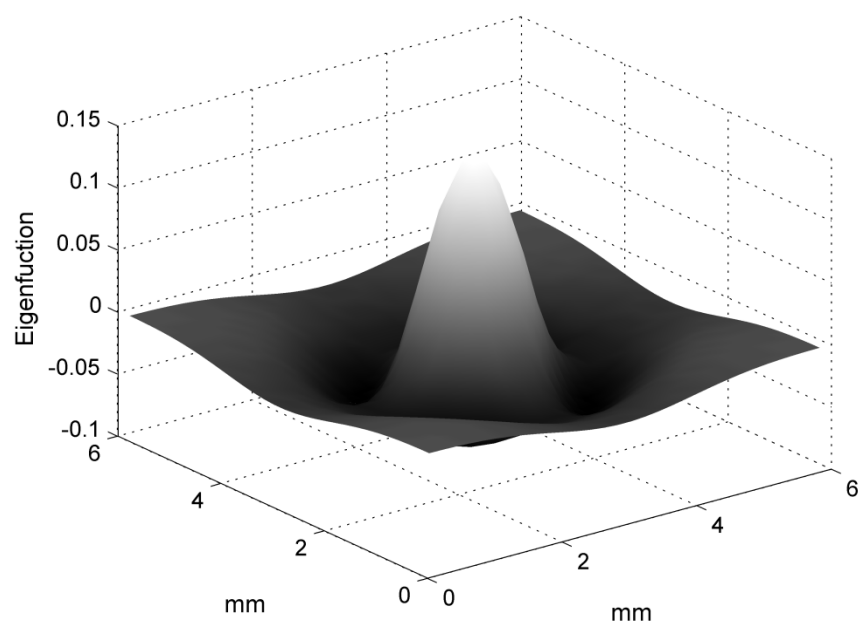


Table 3. Estimated values for thermal parameters. True values are  $\beta_1 = 0.0061 s^{-1}$ ,  $\alpha_1 = 1.1552 \times 10^{-7} m^2.s^{-1}$ ,  $\beta_2 = 0.0202 s^{-1}$  and  $\alpha_2 = 5.0505 \times 10^{-7} m^2.s^{-1}$ .

	Noise amplitude (°C)		
	$\pm 0.50$	$\pm 0.10$	$\pm 0.02$
$\hat{\beta}_1 (s^{-1})$	0.0062	0.0061	0.0061
$ (\beta_1 - \hat{\beta}_1) / \beta_1  \times 100$	2.25	0.58	0.09
$\hat{\beta}_2 (s^{-1})$	0.0208	0.0203	0.0202
$ (\beta_2 - \hat{\beta}_2) / \beta_2  \times 100$	2.77	0.57	0.09
$\hat{\alpha}_1 (\times 10^{-6} m^2 s^{-1})$	0.1524	0.1526	0.1511
$ (\alpha_1 - \hat{\alpha}_1) / \alpha_1  \times 100$	0.60	0.73	0.23
$\hat{\alpha}_2 (\times 10^{-6} m^2 s^{-1})$	0.5001	0.5049	0.5044
$ (\alpha_2 - \hat{\alpha}_2) / \alpha_2  \times 100$	1.00	0.03	0.12

## Many other tests required

Microstructure  
(phase fractions, topology, sizes, etc.)  
Thermal properties (values & contrast)  
Initial thermal field

## Testing CI-SVD method

On-going research with  
Modal-SVD approach



# Other open questions

- How to deal with low resolution images
- Temperature dependent properties
- Sensitivity to the interface location
- Retrieving interfaces at the under-pixel scale
- Estimation of thermal properties at the interfaces
- Point dependent thermal properties (ex:  $\alpha(x,y)$ )
- Initial thermal field providing maximum sensitivity (experiment design)

*E. Palomo del Barrio & Jean-Luc Dauvergne, Chapter 14: Karhunen-Loève decomposition for data, noise, and model reduction in inverse problems, pp. 507-539, in Thermal Measurements and Inverse Techniques, Publisher: CRC Press, Editors: H. RB. Orlande, O. Fudym, D. Maillet, R.M. Cotta, 756 pages, 2011.*